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How to plan your rigid frame building

You can get 529 possible designs out of this manual. All are based on safety and economy and provide the most workable shapes and sizes. Other spans are possible, but will require a complete structural analysis.

At this beginning stage — plan carefully. It will pay off in the long run, eliminating problems before they even come up.

Area planning

Area planning is the basic step toward a useful, adequate building. Plan enough space for work areas, equipment, furnishings and room partitioning. Try to make the area adaptable for any future change-over to another purpose. Keep in mind that in clear span construction, long narrow types are more economical than the more nearly square versions.

As with any building, the site should be selected carefully. Consideration must be given to the slope of the land, relation to other buildings and ease of access.

Planning the frame shape

After the area has been determined, a frame shape and leg height are selected. These play an important part in the overall function of the rigid frame building. Here the enclosed room volume and storage capacity is determined. With the option of either a vertical or slant shape, the resulting design can differ in both usability and economy.

Of the two, the vertical shape is more conventional in appearance but requires the use of heavier frames than those used for a slant shape with the same load and span conditions. The slant leg is more efficient structurally; however, the slant leg shape reduces storage volume when compared to an equal span vertical leg structure.

In many instances, the function of a building may call for vertical inside walls. In these cases, keep the leg height to a minimum to take advantage of the resulting smaller frame material sizes. Extending the leg height of a vertical walled rigid frame unit will increase the stress in the members and may require that they be of a larger size.

On the other hand, as the slant leg height increases, the rigid frame approaches a more efficient structural shape. Thus, in some cases, smaller, less costly member sizes may be used. This may not apply in some cases where the member size is dic-

tated primarily by the wind load rather than the vertical load.

Spacing and loading

Clearly, the greater the spacing between the frames, the fewer the number of frames required. However, plan several spacings — the decreased cost in framing may be offset by the thicker roof sheathing required by the increased spacing.

The loading values used in the tables throughout this manual are the sum of the roofing materials plus the snow load. Be certain to select loads that are realistic.

The use of light loads to justify a marginal design is risky and should never be done. Likewise, it is just as foolish to use excessive design loads. Unnecessary loads result in overbuilding and higher costs.

In any case, comparison of your design with the local building code is a must. Be certain to get the actual local snow load value. Also make sure the requirement for wind pressure design does not exceed the maximum allowable for these rigid frame designs (20 psf).

Doorways

Doorways and other openings should be planned to work with the area, shape and framing. End wall openings offer the easiest approach. Because the end walls bear no load, imaginative treatments not allowable in conventional framing may be applied to the rigid frame structure.

Side doors can be included as a part of the design, although they present engineering and construction problems that are sometimes difficult to work out. Any openings in the side of the rigid frame building involve moving or cutting of the frame units and extreme care must be taken to preserve adequate anchorage, foundation and reinforcement to the adjacent frames.

One of the easiest methods to use in constructing a side entrance, without redesigning the frame unit, is to group the frames at the door sides and span the opening with purlins.

Design conditions

To aid in the design of your rigid frame building, a design example and work sheet follow, illustrating the use of the tables on member sizes, framing details, roofing, wall sheathing and anchorage.

In developing the tables and designs, these conditions were used:

1. Recommended grades for plywood gussets are STRUCTURAL I (A-C, C-C, C-D) or C-C Exterior, depending on moisture conditions and desired appearance.
2. Lumber is stress-graded, with an allowable bending stress of at least 1200 psi throughout its length. Grades meeting this stress level include No. 2 Douglas fir or larch, No. 2 KD southern pine and No. 1 'hem-fir.'
3. Duration of load stress increases have been applied in computations. A 15% increase for snow load and a 33-1/3% increase for wind load were used.
4. The rigid frame building is designed to withstand a 20 psf wind load. This is equivalent to an 80 mph wind and as such, is an adequate value in all areas except those where hurri-

canes or tornados may be expected.

5. The rigid frame building will carry the total roof load shown in the tables. This includes dead load (structure and roofing) plus any live load (snow, etc.).

Foundation design

This publication contains all the information required to design a rigid frame building from the sills upward, as long as it is within the span and load limitations covered. Also included are the forces which must be resisted by the foundation. Design of the foundation requires knowledge of the local soil conditions.

Plywood sheathing required

The frame designs are predicated on the use of plywood as structural elements in the roof decking, wall sheathing and gusset plates. An absolute requirement for a rigid frame building is the use of plywood sheathing. Only plywood will develop the added stiffness essential to the frame members. *Substitution of other materials could result in an unsafe structure.* Complete technical information and design data can be obtained by writing to the American Plywood Association, P.O. Box 11700, Tacoma, Washington 98411, Attention: Technical Services Division.

Note: Current APA nomenclature for C-D and C-C panels is Rated Sheathing. C-D panels are classified Exposure 1 or Exposure 2 and C-C panels are classified Exterior. Structural I panels are so marked. For gussets use only plywood panels which include the notation PS 1-74 in their trademarks.

Design example

1. Required:

A 36' span machine shed with an 8' side wall height.
Vertical side walls are preferred.
Location: Near Atlanta, Georgia.

2. Loads:

Local inquiry to building officials reveals that the 20 psf wind load design for the rigid frames in this manual is satisfactory for the region.

Using a dead load of 5 psf added to the 10 psf snow load totals 15 psf. This value will be used in the selection of the member sizes and roof decking.

3. Selection of member sizes:

Select the member size and spacing from tables on page 6. In the 36' span column, and opposite the 15 psi roof load entries, locate the options for an 8' side wall height. A 24" frame spacing is satisfactory for a farm building.

Frame spacing is often governed by the most economical thickness of plywood for roof sheathing and wall siding.

When no increase is required in sheathing thickness, it is usually more economical to specify heavier frames at a wider spacing.

Also check the member selection table. It's quite possible that the same member size will enclose a higher or wider building.

Final choice:

36' span

8' side wall height (vertical side wall)

24" o.c. frame spacing

2x10 frame members

4. Layout and fabrication details:

The details for cutting and fabricating the frame members and gussets are shown on page 14. They apply to all vertical leg frames made from 2x10 members.

The 8' frame leg — which is called for in this design — is cut at a 5:12 slope on the upper end, and the rafter length (for a 36' span) is 21'-2". However, assume 22' long 2x10's are not available, so the optional splice must be employed to obtain the desired length. An 8' and a 14' member will do.

5. Determining the base anchorage:

In rigid frame structures, certain thrusts must be resisted. The tables on page 9 give the values to be used. In this design example, the values are:

An outward thrust of 330 lbs.,

An inward thrust of 318 lbs., and

An uplift of 75 lbs. at each frame leg.

The anchorage details, page 10, show that one framing anchor, well nailed to the leg and sill, will serve as sufficient anchorage to resist these forces. The sill should then be fastened to the foundation with 1/2" anchor bolts spaced 2' o.c. as shown.

6. Foundation design:

Several suitable foundations are discussed on page 8. Each case varies, of course, with such details as the building's use, the soil, and the climate. Thus, it is difficult to design a correct foundation without complete knowledge of local conditions.



For these reasons, American Plywood Association cannot assume any responsibility for the foundation design. It is suggested that a local engineer or other authority be consulted on its design. The thrust values on page 9 will aid him in developing a satisfactory foundation.

7. Finishing details:

Selecting and detailing the windows, the plywood siding and doors and other finish items will complete the design.

Worksheet

1. General information

Shape  ☒  ☐
 Span 36'-0"
 Frame spacing 24" o.c.
 Leg Length 8'-0"

Bldg. Use Farm Machine Shed
 Roof load D.L. 5 PSF
 Snow load 10 PSF
 TOTAL 15 PSF
 (Wind load 20 PSF)

2. Member size: 2"X10" (Leg & rafters)

Grade: (Must have allowable bending stress of 1200 psi throughout)

Rafter length: 21'-2" Leg length: 8'-0"

No. 2 KD Southern Pine

3. Plywood (APA)

	THICKNESS	IDENTIFICATION INDEX*	APA GRADE
Gussets: Haunch	<u>1/2"</u>		C-C EXT <input checked="" type="checkbox"/> STRUCT 1: AC <input type="checkbox"/> C-C <input type="checkbox"/> C-D <input type="checkbox"/>
Crown	<u>1/2"</u>		C-C EXT <input checked="" type="checkbox"/> STRUCT 1: AC <input type="checkbox"/> C-C <input type="checkbox"/> C-D <input type="checkbox"/>
Combination Wall Siding-Sheathing	<u>3/8"</u>		C-C EXT <input checked="" type="checkbox"/> B-C EXT <input type="checkbox"/> A-C EXT <input type="checkbox"/> Texture 1-11 <input type="checkbox"/> 303 Siding <input type="checkbox"/> Medium Density Overlaid Plywood <input type="checkbox"/>
Inside Finish	<u>NONE</u>		C-D INT <input type="checkbox"/> C-D INT exterior glue <input type="checkbox"/> C-C EXT <input type="checkbox"/> B-C EXT <input type="checkbox"/> A-C EXT <input type="checkbox"/>
Roof Decking	<u>3/8"</u>	<u>24/0</u>	C-D INT <input type="checkbox"/> C-D INT exterior glue <input type="checkbox"/> C-C EXT <input checked="" type="checkbox"/> B-C EXT <input type="checkbox"/> A-C EXT <input type="checkbox"/>

*Required for roof deck only

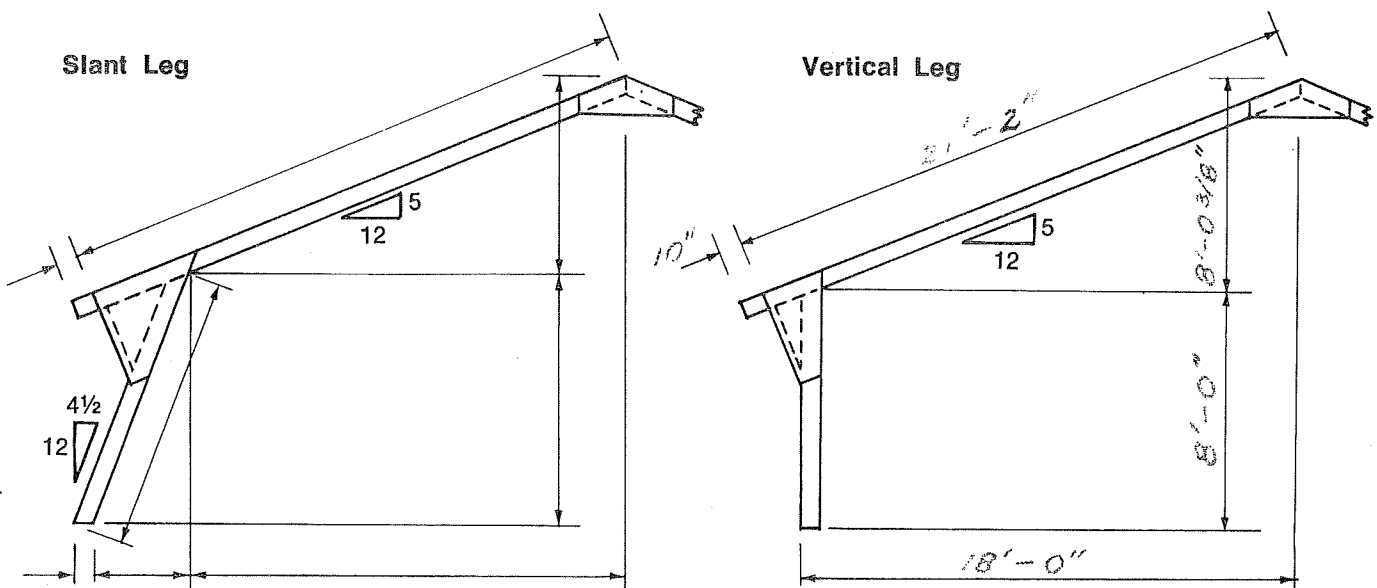
4. Reactions for use in anchorage and foundation design (see page 9)

Outward 330 lb.
 Inward 318 lb.
 Upward 75 lb.

Down = $\frac{\text{span} \times \text{spacing} \times \text{loading}}{2} = \frac{36' \times 24" \times 15 \text{ PSF}}{2} = \underline{540}$ lb.†

†Required for foundation design only

5. Construction details for this building were taken from page 14



Member selection table

vertical leg

24' SPAN

Total Roof Load	Leg Height	16"	Frame Spacing, o.c.		
			24"	32"	48"
15 PSF	6'	2x6	2x8	2x8	2x10
	8'	2x8	2x8	2x10	2x12
	10'	2x8	2x10	2x12	—
	12'	2x10	2x10	2x12	—
20 PSF	6'	2x6	2x8	2x10	2x12
	8'	2x8	2x8	2x10	2x12
	10'	2x8	2x10	2x12	—
	12'	2x10	2x10	2x12	—
25 PSF	6'	2x8	2x8	2x10	2x12
	8'	2x8	2x8	2x10	2x12
	10'	2x8	2x10	2x12	—
	12'	2x10	2x10	2x12	—
35 PSF	6'	2x8	2x10	2x12	—
	8'	2x8	2x10	2x12	—
	10'	2x8	2x10	2x12	—
	12'	2x10	2x10	2x12	—
50 PSF	6'	2x10	2x12	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x12	—	—
	12'	2x10	2x12	—	—

32' SPAN

Total Roof Load	Leg Height	16"	Frame Spacing, o.c.		
			24"	32"	48"
15 PSF	6'	2x8	2x8	2x10	2x12
	8'	2x8	2x10	2x12	—
	10'	2x10	2x12	2x12	—
	12'	2x10	2x12	—	—
20 PSF	6'	2x8	2x10	2x12	—
	8'	2x8	2x10	2x12	—
	10'	2x10	2x12	2x12	—
	12'	2x10	2x12	—	—
25 PSF	6'	2x10	2x12	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x12	—	—
	12'	2x10	2x12	—	—
35 PSF	6'	2x10	2x12	—	—
	8'	2x10	—	—	—
	10'	2x12	—	—	—
	12'	2x12	—	—	—
50 PSF	6'	2x12	—	—	—
	8'	2x12	—	—	—
	10'	2x12	—	—	—
	12'	2x12	—	—	—

36' SPAN

Total Roof Load	Leg Height	16"	Frame Spacing, o.c.		
			24"	32"	48"
15 PSF	6'	2x8	2x10	2x12	—
	8'	2x8	2x10	2x12	—
	10'	2x10	2x12	—	—
	12'	2x10	2x12	—	—
20 PSF	6'	2x10	2x12	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x12	—	—
	12'	2x10	2x12	—	—
25 PSF	6'	2x10	2x12	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x12	—	—
	12'	2x10	2x12	—	—
35 PSF	6'	2x12	—	—	—
	8'	2x12	—	—	—
	10'	2x12	—	—	—
	12'	2x12	—	—	—
50 PSF	6'	—	—	—	—
	8'	—	—	—	—
	10'	—	—	—	—
	12'	—	—	—	—

40' SPAN

Total Roof Load	Leg Height	16"	Frame Spacing, o.c.		
			24"	32"	48"
15 PSF	6'	2x8	2x10	2x12	—
	8'	2x10	2x10	2x12	—
	10'	2x10	2x12	—	—
	12'	2x10	2x12	—	—
20 PSF	6'	2x10	2x12	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x12	—	—
	12'	2x10	2x12	—	—
25 PSF	6'	2x10	—	—	—
	8'	2x12	—	—	—
	10'	2x12	—	—	—
	12'	2x12	—	—	—
35 PSF	6'	2x12	—	—	—
	8'	—	—	—	—
	10'	—	—	—	—
	12'	—	—	—	—
50 PSF	6'	—	—	—	—
	8'	—	—	—	—
	10'	—	—	—	—
	12'	—	—	—	—

44' SPAN

Total Roof Load	Leg Height	16"	Frame Spacing, o.c.		
			24"	32"	48"
15 PSF	6'	2x10	2x12	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x12	—	—
	12'	2x12	—	—	—
20 PSF	6'	2x10	2x12	—	—
	8'	2x12	—	—	—
	10'	2x12	—	—	—
	12'	2x12	—	—	—
25 PSF	6'	2x12	—	—	—
	8'	2x12	—	—	—
	10'	2x12	—	—	—
	12'	2x12	—	—	—
35 PSF	6'	—	—	—	—
	8'	—	—	—	—
	10'	—	—	—	—
	12'	—	—	—	—
50 PSF	6'	—	—	—	—
	8'	—	—	—	—
	10'	—	—	—	—
	12'	—	—	—	—

48' SPAN

Total Roof Load	Leg Height	16"	Frame Spacing, o.c.		
			24"	32"	48"
15 PSF	6'	2x10	2x12	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x12	—	—
	12'	2x12	—	—	—
20 PSF	6'	2x12	—	—	—
	8'	2x12	—	—	—
	10'	2x12	—	—	—
	12'	2x12	—	—	—
25 PSF	6'	2x12	—	—	—
	8'	2x12	—	—	—
	10'	—	—	—	—
	12'	—	—	—	—
35 PSF	6'	—	—	—	—
	8'	—	—	—	—
	10'	—	—	—	—
	12'	—	—	—	—
50 PSF	6'	—	—	—	—
	8'	—	—	—	—
	10'	—	—	—	—
	12'	—	—	—	—

Member selection table

slant leg

24' SPAN

Total Roof Load	Leg Height	16"	Frame Spacing, o.c.		
			24"	32"	48"
15 PSF	6'	2x6	2x6	2x6	2x8
	8'	2x6	2x6	2x8	2x8
	10'	2x6	2x8	2x8	2x10
	12'	2x6	2x8	2x8	2x10
20 PSF	6'	2x6	2x6	2x6	2x8
	8'	2x6	2x6	2x8	2x8
	10'	2x6	2x8	2x8	2x10
	12'	2x6	2x8	2x8	2x10
25 PSF	6'	2x6	2x6	2x8	2x10
	8'	2x6	2x6	2x8	2x8
	10'	2x6	2x8	2x8	2x10
	12'	2x6	2x8	2x8	2x10
35 PSF	6'	2x6	2x8	2x8	2x10
	8'	2x6	2x8	2x8	2x10
	10'	2x6	2x8	2x8	2x10
	12'	2x6	2x8	2x8	2x10
50 PSF	6'	2x8	2x8	2x10	2x12
	8'	2x8	2x8	2x10	2x12
	10'	2x6	2x8	2x10	2x12
	12'	2x6	2x8	2x8	2x10

32' SPAN

Total Roof Load	Leg Height	16"	Frame Spacing, o.c.		
			24"	32"	48"
15 PSF	6'	2x6	2x8	2x8	2x10
	8'	2x6	2x8	2x8	2x10
	10'	2x6	2x8	2x10	2x12
	12'	2x8	2x8	2x10	2x12
20 PSF	6'	2x6	2x8	2x10	2x12
	8'	2x6	2x8	2x10	2x10
	10'	2x6	2x8	2x10	2x12
	12'	2x8	2x8	2x10	2x12
25 PSF	6'	2x8	2x8	2x10	2x12
	8'	2x8	2x8	2x10	2x12
	10'	2x6	2x8	2x10	2x12
	12'	2x8	2x8	2x10	2x12
35 PSF	6'	2x8	2x10	2x12	—
	8'	2x8	2x10	2x12	—
	10'	2x8	2x10	2x12	—
	12'	2x8	2x8	2x10	2x12
50 PSF	6'	2x10	2x12	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x10	2x12	—
	12'	2x8	2x10	2x12	—

36' SPAN

Total Roof Load	Leg Height	16"	Frame Spacing, o.c.		
			24"	32"	48"
15 PSF	6'	2x6	2x8	2x10	2x10
	8'	2x6	2x8	2x10	2x12
	10'	2x8	2x8	2x10	2x12
	12'	2x8	2x10	2x10	2x12
20 PSF	6'	2x8	2x8	2x10	2x12
	8'	2x8	2x8	2x10	2x12
	10'	2x8	2x8	2x10	2x12
	12'	2x8	2x10	2x10	2x12
25 PSF	6'	2x8	2x10	2x12	—
	8'	2x8	2x10	2x12	—
	10'	2x8	2x10	2x12	2x12
	12'	2x8	2x10	2x10	2x12
35 PSF	6'	2x10	2x10	2x12	—
	8'	2x10	2x10	2x12	—
	10'	2x8	2x10	2x12	—
	12'	2x8	2x10	2x12	—
50 PSF	6'	2x10	—	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x12	—	—
	12'	2x10	2x12	—	—

40' SPAN

Total Roof Load	Leg Height	16"	Frame Spacing, o.c.		
			24"	32"	48"
15 PSF	6'	2x8	2x8	2x10	2x12
	8'	2x8	2x8	2x10	2x12
	10'	2x8	2x10	2x10	2x12
	12'	2x8	2x10	2x12	—
20 PSF	6'	2x8	2x10	2x12	—
	8'	2x8	2x10	2x12	—
	10'	2x8	2x10	2x10	—
	12'	2x8	2x10	2x12	—
25 PSF	6'	2x8	2x10	2x12	—
	8'	2x8	2x10	2x12	—
	10'	2x8	2x10	2x12	—
	12'	2x8	2x10	2x12	—
35 PSF	6'	2x10	2x12	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x12	—	—
	12'	2x10	2x12	—	—
50 PSF	6'	2x12	—	—	—
	8'	2x12	—	—	—
	10'	2x12	—	—	—
	12'	2x12	—	—	—

44' SPAN

Total Roof Load	Leg Height	16"	Frame Spacing, o.c.		
			24"	32"	48"
15 PSF	6'	2x8	2x10	2x10	2x12
	8'	2x8	2x10	2x10	2x12
	10'	2x8	2x10	2x12	—
	12'	2x8	2x10	2x12	—
20 PSF	6'	2x8	2x10	2x12	—
	8'	2x8	2x10	2x12	—
	10'	2x8	2x10	2x12	—
	12'	2x8	2x10	2x12	—
25 PSF	6'	2x10	2x12	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x12	—	—
	12'	2x10	2x10	2x12	—
35 PSF	6'	2x12	—	—	—
	8'	2x12	—	—	—
	10'	2x10	—	—	—
	12'	2x10	2x12	—	—
50 PSF	6'	2x12	—	—	—
	8'	2x12	—	—	—
	10'	2x12	—	—	—
	12'	2x12	—	—	—

48' SPAN

Total Roof Load	Leg Height	16"	Frame Spacing, o.c.		
			24"	32"	48"
15 PSF	6'	2x8	2x10	2x12	—
	8'	2x8	2x10	2x12	—
	10'	2x8	2x10	2x12	—
	12'	2x10	2x10	2x12	—
20 PSF	6'	2x10	2x12	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x12	—	—
	12'	2x10	2x10	2x12	—
25 PSF	6'	2x10	2x12	—	—
	8'	2x10	2x12	—	—
	10'	2x10	2x12	—	—
	12'	2x10	2x12	—	—
35 PSF	6'	2x12	—	—	—
	8'	2x12	—	—	—
	10'	2x12	—	—	—
	12'	2x12	—	—	—
50 PSF	6'	—	—	—	—
	8'	—	—	—	—
	10'	—	—	—	—
	12'	—	—	—	—

Thrust, foundation and anchorage

A characteristic of the rigid frame, not found in many framing systems, is the thrust type of force.

The rigid frame develops an outward thrust similar to an arch, a moderate inward force plus a small uplift. The outward thrust is caused by the weight of the building and any snow load on the roof. The inward and uplift forces are due to the action of the wind on the sides of the building.

The designers of the rigid frames have provided the building strength and rigidity required through the use of plywood. But sound rigid frame buildings also depend upon good foundations and special leg anchorage.

Foundation type

Foundation types and sizes vary with the building use, soil type, climate and building code requirements. Because of this, you will need to obtain the services of a qualified builder or engineer to prepare the foundation design. The thrust tables will aid the designer in developing a satisfactory design.

Some of the popular methods used as foundations for the rigid frame employ the use of a "cross-tie" system. The slab-foundation acts as a tie rod to join the walls so the thrust of one counteracts the other. For rigid frames with wood floors, floor joists can be

designed to act in the same way. When no floor is planned, a buttress or gravity type wall foundation will serve well when properly designed.

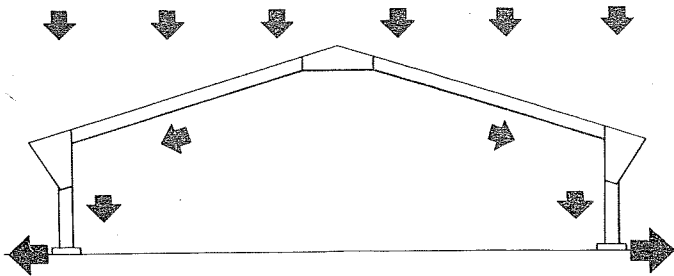
Anchorage

Anchoring the studs to the foundation is critical. Toe-nailing them to the sill plate is not adequate and could result in a failure of the frame support. Framing anchors shown in the illustrations on page 10 have known load bearing capacities. Wrap-around or bent plate fasteners are suitable, but care must be taken to use an adequate number of nails.

The anchorage details on page 10 are suitable for either the slant or vertical leg versions.

Thrust Tables

■ Vertical Leg



**Maximum Base Reaction
Horizontal Thrust—Outward (lbs./Frame Leg)**

Leg Height	Member Size			
	2 x 6	2 x 8	2 x 10	2 x 12
6'	150	275	440	640
8'	—	210	330	480
10'	—	170	270	390
12'	—	140	220	330

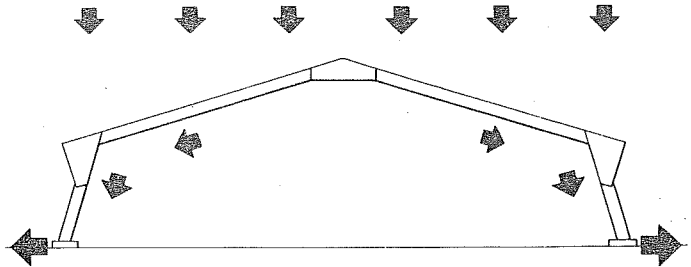
**Maximum Base Reaction
Horizontal Thrust—Inward (lbs./Frame Leg)**

Leg Height	Frame Spacing			
	16"	24"	32"	48"
6'	161	241	322	483
8'	212	318	424	637
10'	262	392	523	785
12'	308	462	616	924

**Maximum Uplift (lbs./Frame Leg)
Vertical and Slant Leg Values**

Frame Spacing	Uplift
16" o.c.	50
24" o.c.	75
32" o.c.	100
48" o.c.	150

▲ Slant Leg



**Maximum Base Reaction
Horizontal Thrust—Outward (lbs./Frame Leg)**

Leg Height	Member Size			
	2 x 6	2 x 8	2 x 10	2 x 12
6'	310	630	880	1290
8'	320	560	840	1260
10'	320	650	970	1100
12'	290	580	870	980

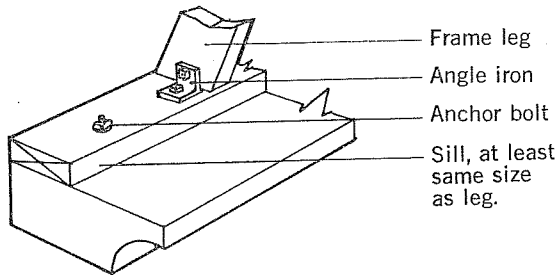
**Maximum Base Reaction
Horizontal Thrust—Inward (lbs./Frame Leg)**

Leg Height	Frame Spacing			
	16"	24"	32"	48"
6'	117	175	234	351
8'	156	234	312	468
10'	195	293	391	587
12'	236	354	472	709

NOTE: In order to keep the thrust table simple, like values have been grouped. The most critical case is shown and as a result construction based on these values will always be safe.

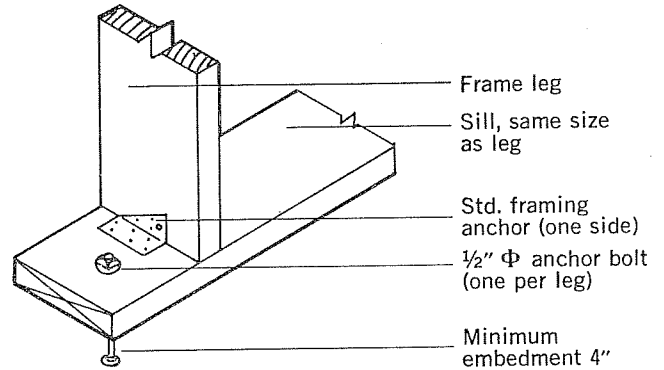
Anchorage details

(Allowable load varies with size and detail of parts)



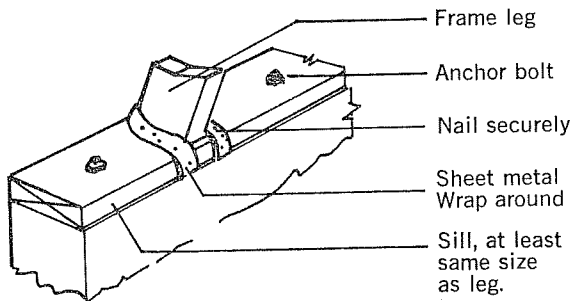
Frame leg
Angle iron
Anchor bolt
Sill, at least same size as leg.

Allowable load 0# to 450#



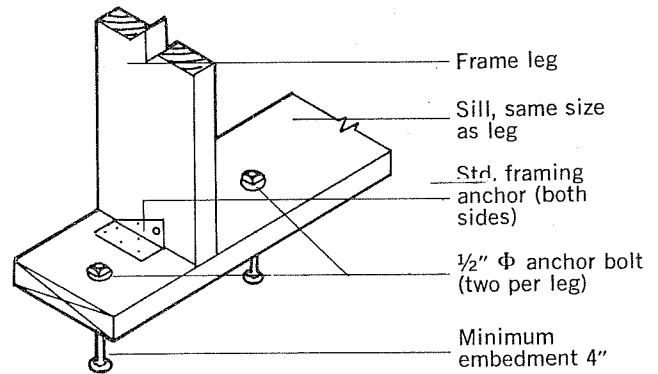
Frame leg
Sill, same size as leg
Std. framing anchor (one side)
1/2" Φ anchor bolt (one per leg)
Minimum embedment 4"

(Allowable load varies with size and detail of parts)



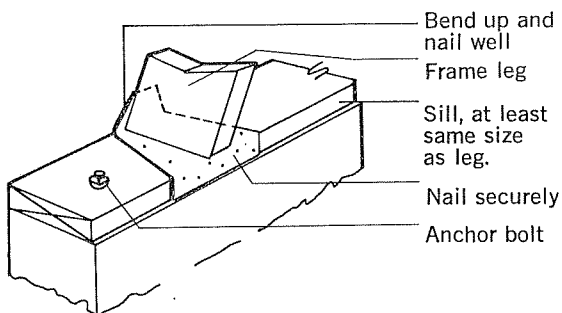
Frame leg
Anchor bolt
Nail securely
Sheet metal Wrap around
Sill, at least same size as leg.

Allowable load 450# to 900#



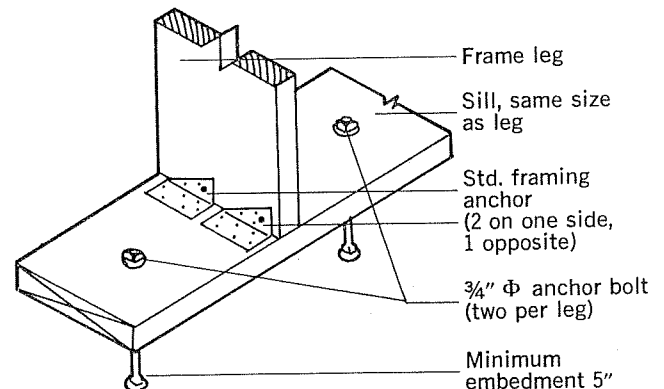
Frame leg
Sill, same size as leg
Std. framing anchor (both sides)
1/2" Φ anchor bolt (two per leg)
Minimum embedment 4"

(Allowable load varies with size and detail of parts)



Bend up and nail well
Frame leg
Sill, at least same size as leg.
Nail securely
Anchor bolt

Allowable load 900# to 1350#



Frame leg
Sill, same size as leg
Std. framing anchor (2 on one side, 1 opposite)
3/4" Φ anchor bolt (two per leg)
Minimum embedment 5"

Frame fabrication details

Note that dimensions correspond to pre-PS 20 net lumber sizes. However, dimensions remain accurate within 1/4".


How to use the fabrication details


The following pages contain plans and information for fabricating and erecting the rigid frame. Frame dimensions and layout may be found by turning to the page that corresponds to the member size and shape selected.

Details for each member size apply to the entire range of spans and leg lengths. Because these details are varied, be sure to take the correct information from the tables and drawings.

The first section of fabrication details pertains to member sizes for vertical leg shapes. The slant leg section follows.

To prevent selecting a member size with the wrong shape, symbols are placed in the page heading.

The vertical leg symbol: 

The slant leg symbol: 

Be sure you have the right page by checking the symbol on the page heading.

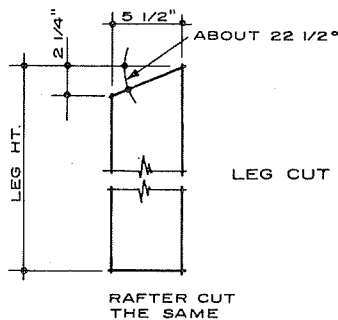
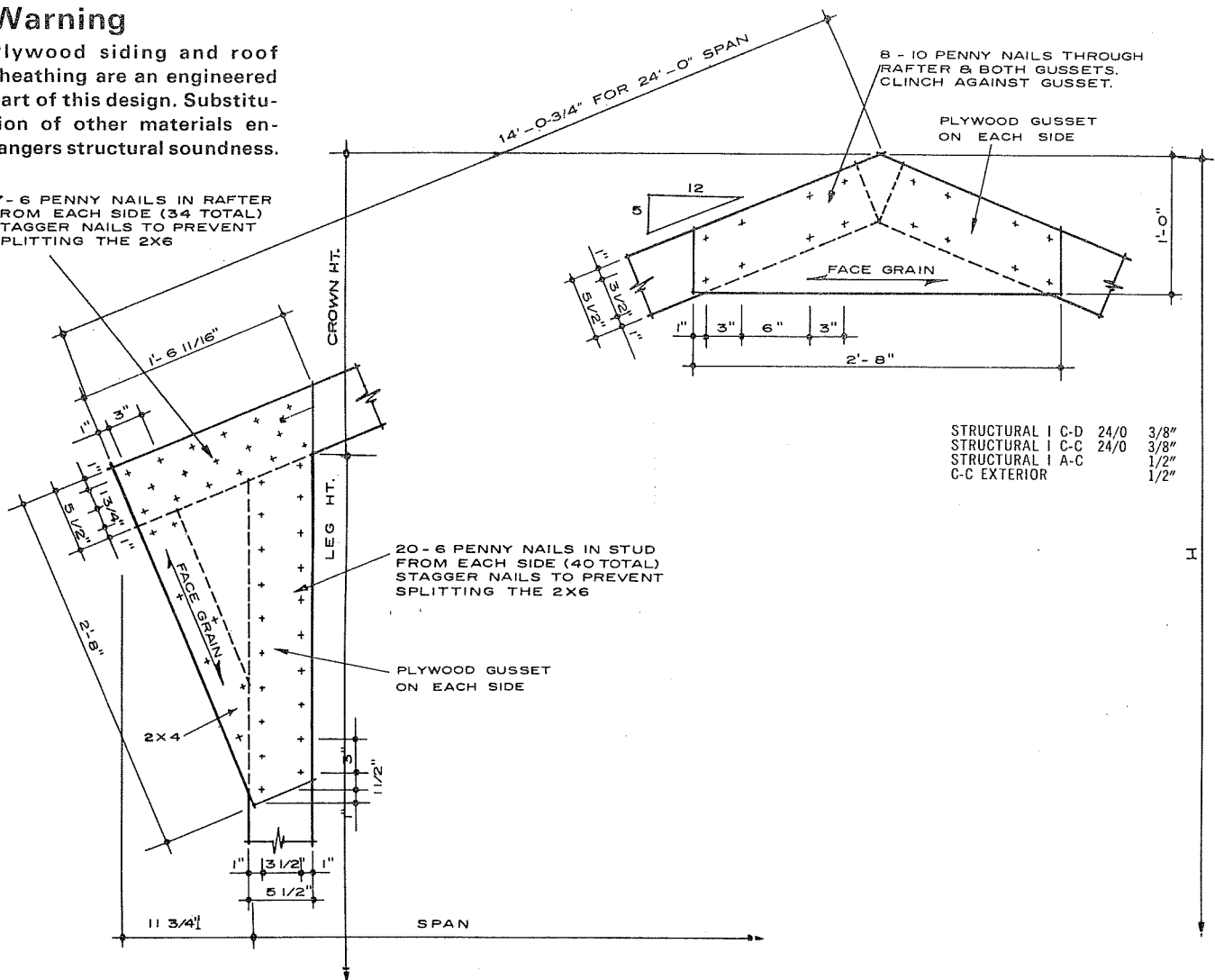
Fabrication details

2x6 vertical leg

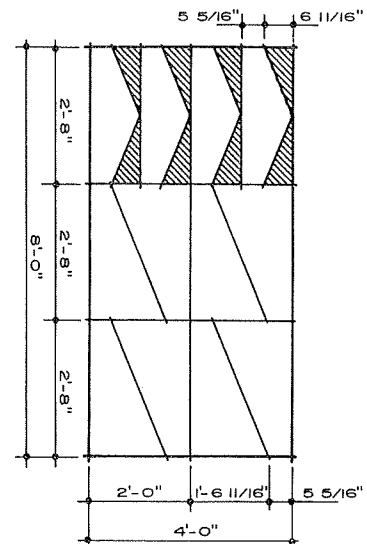
Warning

Plywood siding and roof sheathing are an engineered part of this design. Substitution of other materials endangers structural soundness.

17- 6 PENNY NAILS IN RAFTER FROM EACH SIDE (34 TOTAL) STAGGER NAILS TO PREVENT SPLITTING THE 2X6



Plywood cutting diagram



Frame layout

Span	Crown Height	Leg Height			
		6'	8'	10'	12'
		Overall Dimension (H)			
24'	5'- 3 5/8"	11'- 3 5/8"	13'- 3 5/8"	15'- 3 5/8"	17'- 3 5/8"

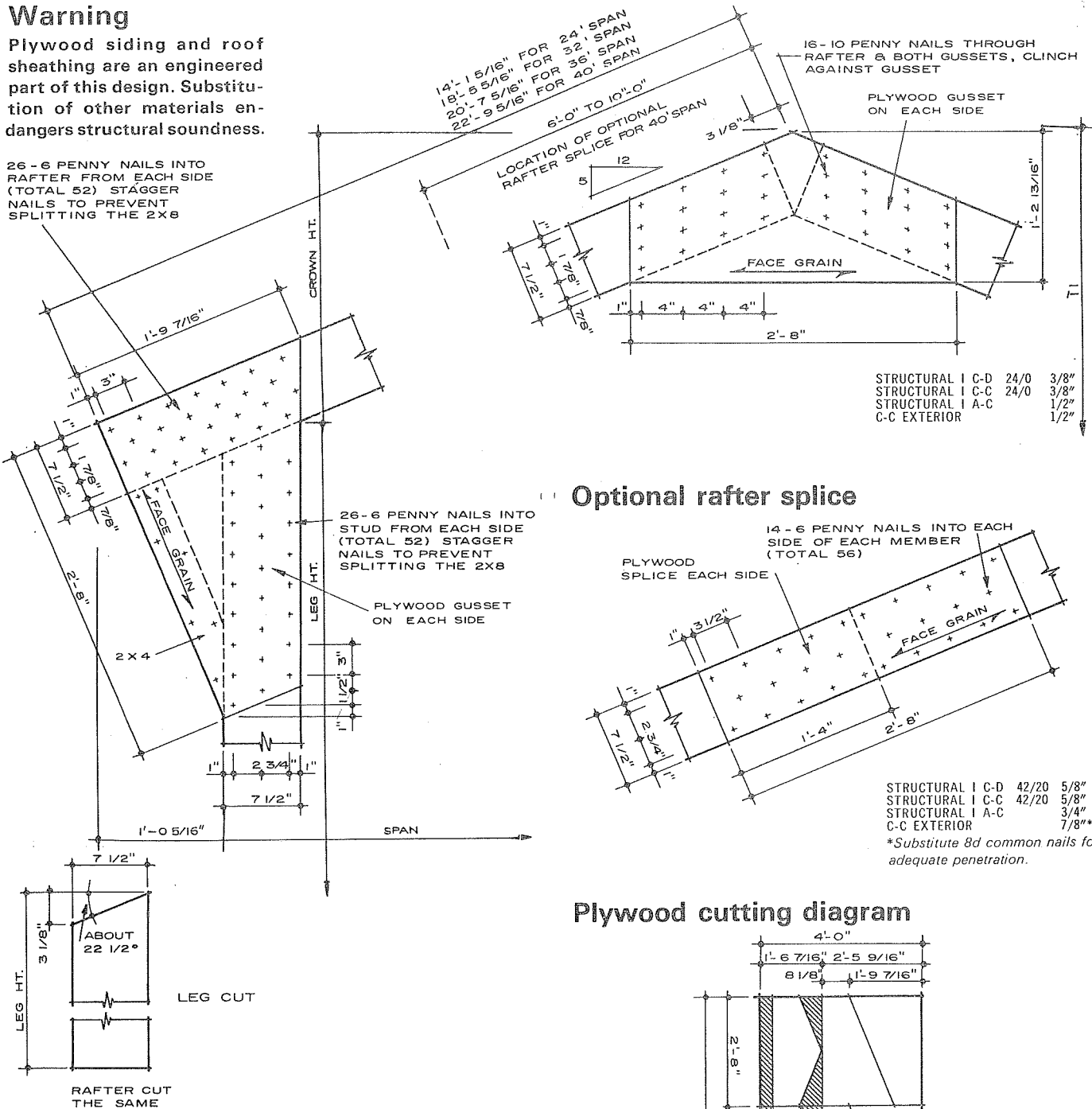
Fabrication details

2x8 vertical leg

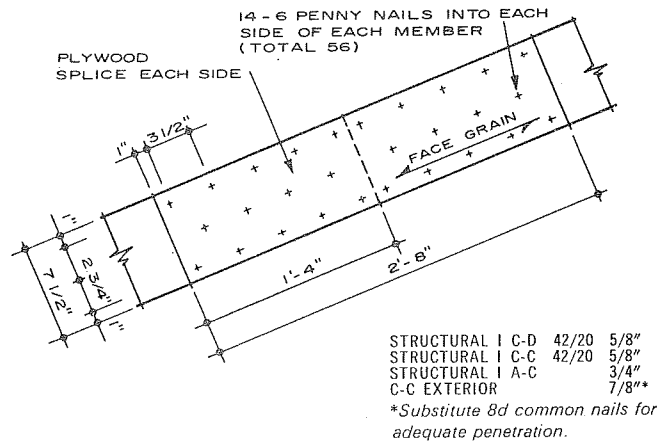
Warning

Plywood siding and roof sheathing are an engineered part of this design. Substitution of other materials endangers structural soundness.

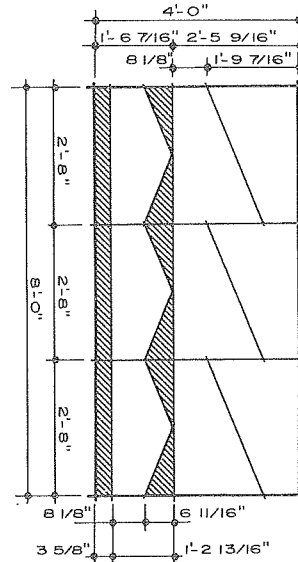
26-6 PENNY NAILS INTO RAFTER FROM EACH SIDE (TOTAL 52) STAGGER NAILS TO PREVENT SPLITTING THE 2X8



Optional rafter splice



Plywood cutting diagram



Frame layout

Span	Crown Height	Leg Height			
		6'	8'	10'	12'
		Overall Dimension (H)			
24'	5'- 5"	11'- 5"	13'- 5"	15'- 5"	17'- 5"
32'	7'- 1"	13'- 1"	15'- 1"	17'- 1"	19'- 1"
36'	7'-11"	13'-11"	15'-11"	17'-11"	19'-11"
40'	8'- 9"	14'- 9"	16'- 9"	18'- 9"	20'- 9"

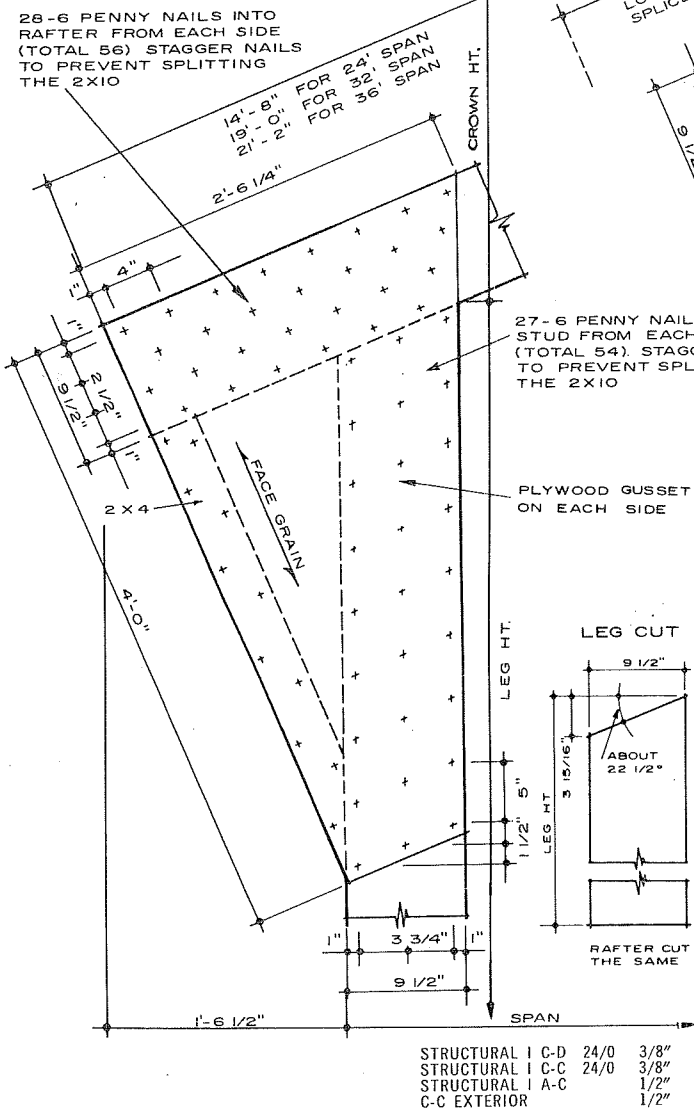
Fabrication details

2x10 vertical leg

Warning

Plywood siding and roof sheathing are an engineered part of this design. Substitution of other materials endangers structural soundness.

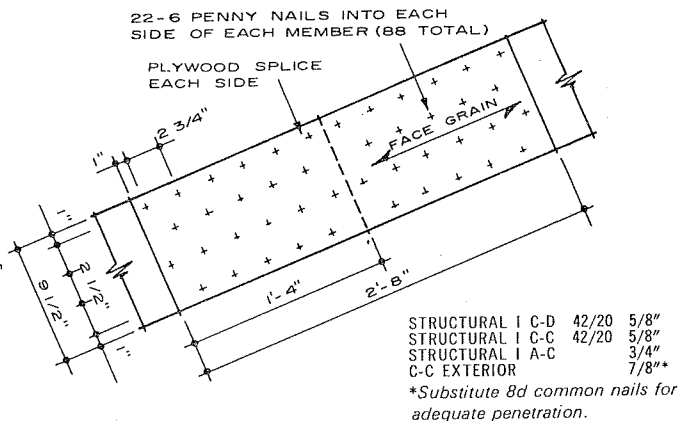
28-6 PENNY NAILS INTO RAFTER FROM EACH SIDE (TOTAL 56) STAGGER NAILS TO PREVENT SPLITTING THE 2X10



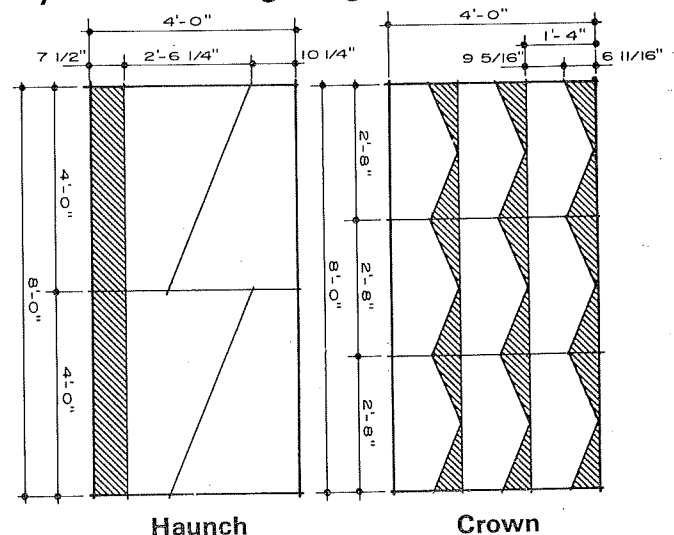
20-10 PENNY NAILS DRIVEN THROUGH RAFTER & BOTH GUSSETS, CLINCH AGAINST GUSSET.

PLYWOOD GUSSET ON EACH SIDE

Optional rafter splice



Plywood cutting diagram



Frame layout

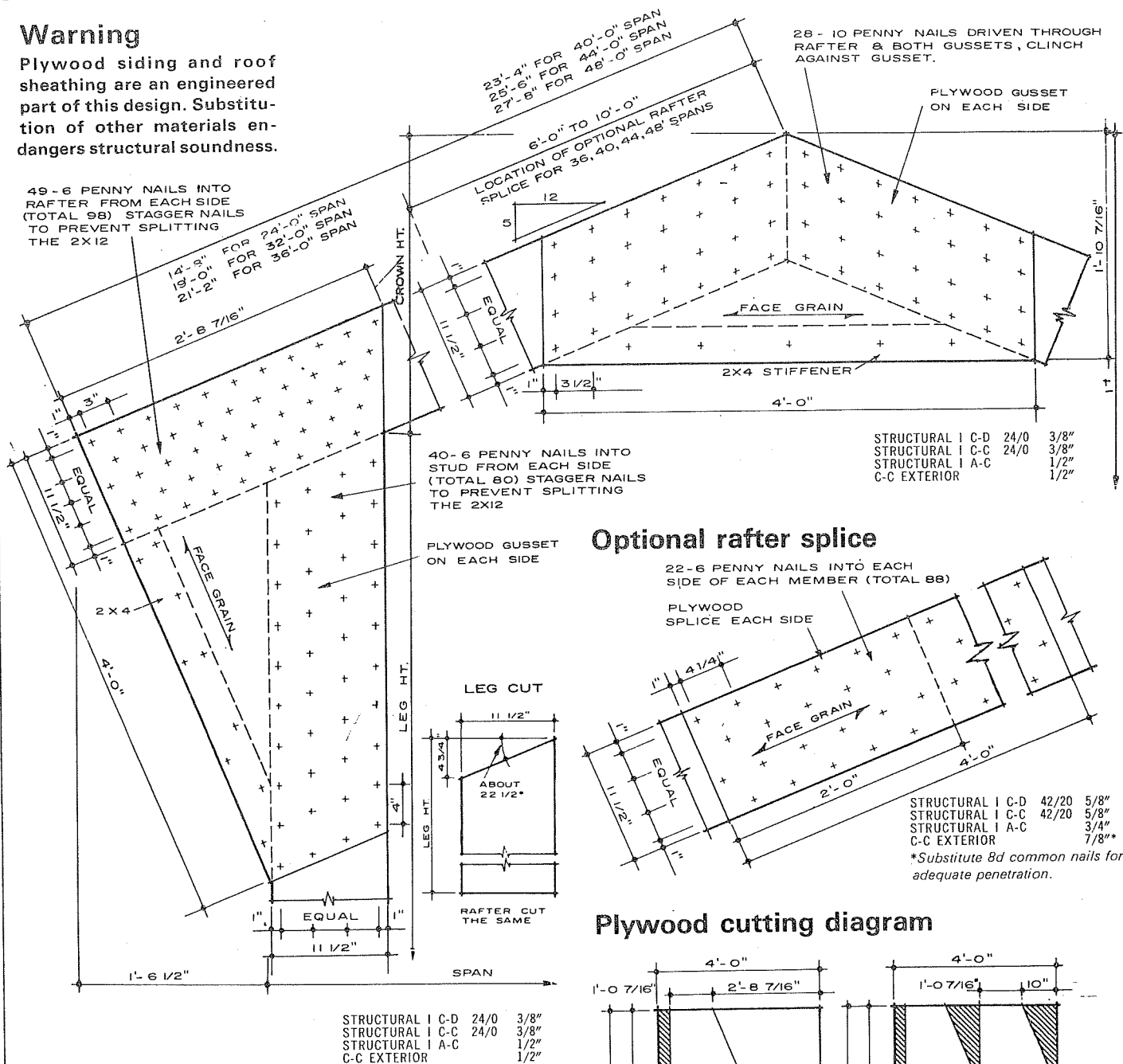
Span	Crown Height	Leg Height			
		6'	8'	10'	12'
		Overall Dimension (H)			
24'	5'- 6¾"	11'- 6¾"	13'- 6¾"	15'- 6¾"	17'- 6¾"
32'	7'- 2¾"	13'- 2¾"	15'- 2¾"	17'- 2¾"	19'- 2¾"
36'	8'- 0¾"	14'- 0¾"	16'- 0¾"	18'- 0¾"	20'- 0¾"
40'	8'-10¾"	14'-10¾"	16'-10¾"	18'-10¾"	20'-10¾"
44'	9'- 8¾"	15'- 8¾"	17'- 8¾"	19'- 8¾"	21'- 8¾"
48'	10'- 6¾"	16'- 6¾"	18'- 6¾"	20'- 6¾"	22'- 6¾"

Fabrication details

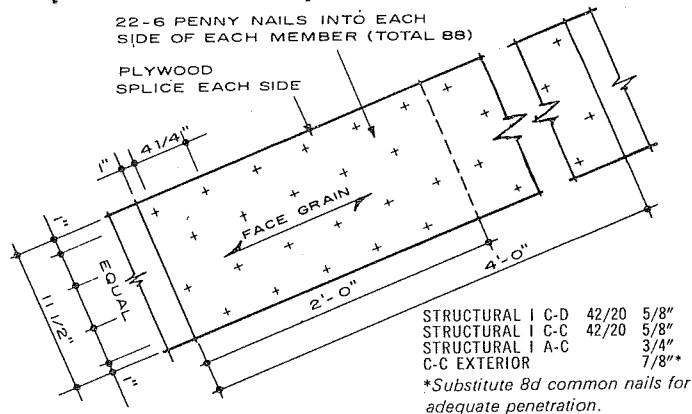
2x12 vertical leg

Warning

Plywood siding and roof sheathing are an engineered part of this design. Substitution of other materials endangers structural soundness.

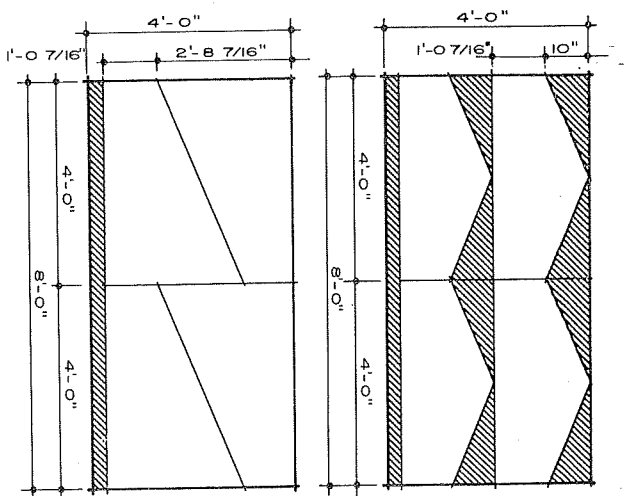


Optional rafter splice



*Substitute 8d common nails for adequate penetration.

Plywood cutting diagram

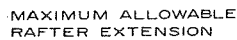


Frame layout

Span	Crown Height	Leg Height			
		6'	8'	10'	12'
		Overall Dimension (H)			
24'	5'- 7½"	11'- 7½"	13'- 7½"	15'- 7½"	17'- 7½"
32'	7'- 3½"	13'- 3½"	15'- 3½"	17'- 3½"	19'- 3½"
36'	8'- 1½"	14'- 1½"	16'- 1½"	18'- 1½"	20'- 1½"
40'	8'-11½"	14'-11½"	16'-11½"	18'-11½"	20'-11½"
44'	9'- 9½"	15'- 9½"	17'- 9½"	19'- 9½"	21'- 9½"
48'	10'- 7½"	16'- 7½"	18'- 7½"	20'- 7½"	22'- 7½"

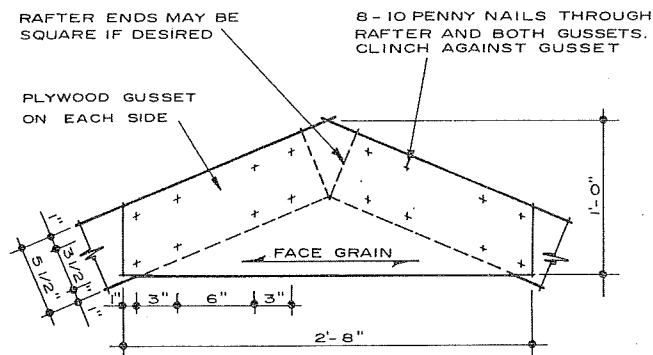
2x6 slant leg

Plywood siding and roof sheathing are an engineered part of this design. Substitution of other materials endangers structural soundness.



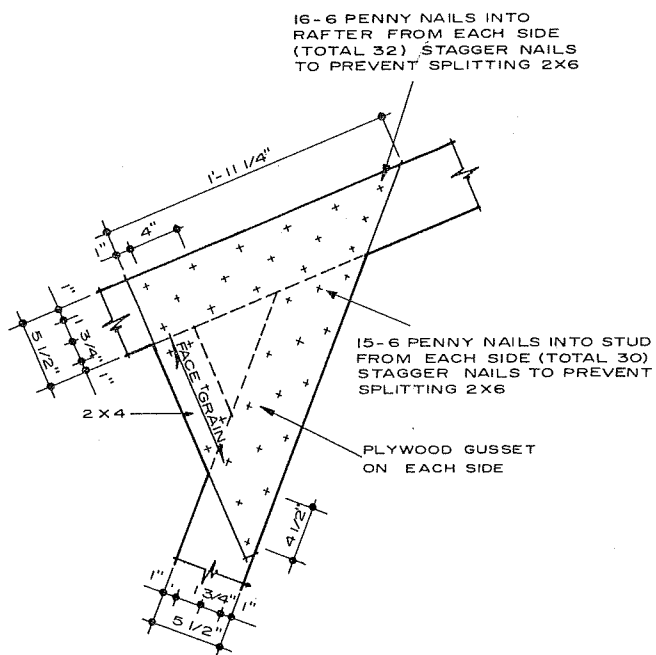
	A	6'- 0"	8'- 0"	10'- 0"	12'- 0"
All	B	2'- 0 ⁷ / ₁₆ "	2'- 9"	3'- 5 ³ / ₈ "	4'- 1 ³ / ₁₆ "
	C	5'- 5 ¹ / ₂ "	7'- 4"	9'- 2 ⁷ / ₁₆ "	11'- 0 ⁷ / ₈ "
	G	1'- 0 ⁹ / ₁₆ "	1'- 9 ¹ / ₁₆ "	2'- 6 ³ / ₄ "	3'- 3 ⁷ / ₈ "
24' span	D	9'- 5 ⁹ / ₁₆ "	8'- 9 ¹ / ₈ "	8'- 0 ³ / ₄ "	7'- 4 ⁵ / ₁₆ "
	E	4'- 5 ¹ / ₄ "	4'- 1 ³ / ₄ "	3'-10 ¹ / ₄ "	3'- 6 ³ / ₄ "
	F	11'-11 ⁷ / ₁₆ "	11'- 2 ⁵ / ₁₆ "	10'- 5 ¹ / ₄ "	9'- 8 ¹ / ₂ "
	H	9'-10 ³ / ₄ "	11'- 5 ³ / ₄ "	13'- 0 ¹ / ₁₆ "	14'- 7 ⁵ / ₈ "
32' span	D	13'- 5 ⁹ / ₁₆ "	12'- 9 ¹ / ₈ "	12'- 0 ³ / ₄ "	
	E	6'- 1 ¹ / ₄ "	5'- 9 ³ / ₄ "	5'- 6 ¹ / ₄ "	
	F	16'- 3 ⁷ / ₁₆ "	15'- 6 ⁵ / ₁₆ "	14'- 9 ¹ / ₄ "	
	H	11'- 6 ³ / ₄ "	13'- 1 ³ / ₄ "	14'- 8 ¹ / ₁₆ "	
36' span	D	15'- 5 ⁹ / ₁₆ "	14'- 9 ¹ / ₈ "		
	E	6'-11 ¹ / ₄ "	6'- 7 ³ / ₄ "		
	F	18'- 5 ⁷ / ₁₆ "	17'- 8 ⁵ / ₁₆ "		
	H	12'- 4 ³ / ₄ "	13'-11 ³ / ₄ "		

Crown gusset detail



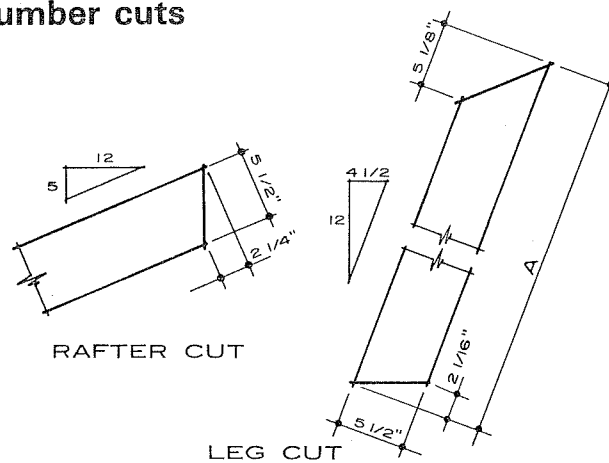
STRUCTURAL I C-D	24/0	3/8"
STRUCTURAL I C-C	24/0	3/8"
STRUCTURAL I A-C		1/2"
C-C EXTERIOR		1/2"

Haunch gusset detail

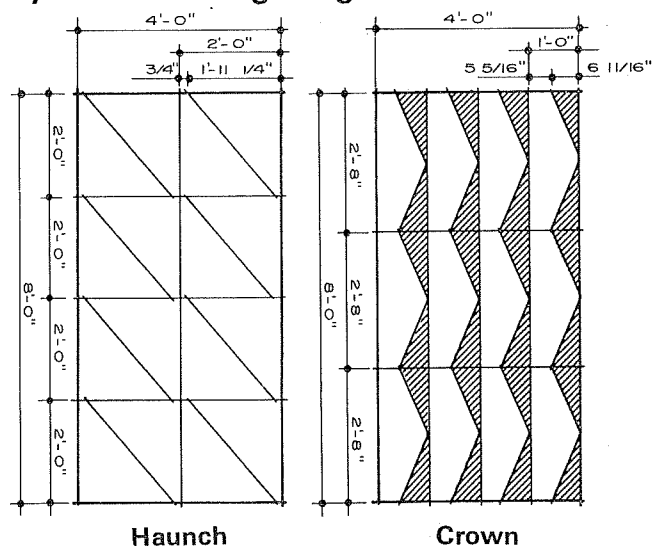


STRUCTURAL I C-D	24/0	3/8"
STRUCTURAL I C-C	24/0	3/8"
STRUCTURAL I A-C		1/2"
C-C EXTERIOR		1/2"

Lumber cuts



Plywood cutting diagram

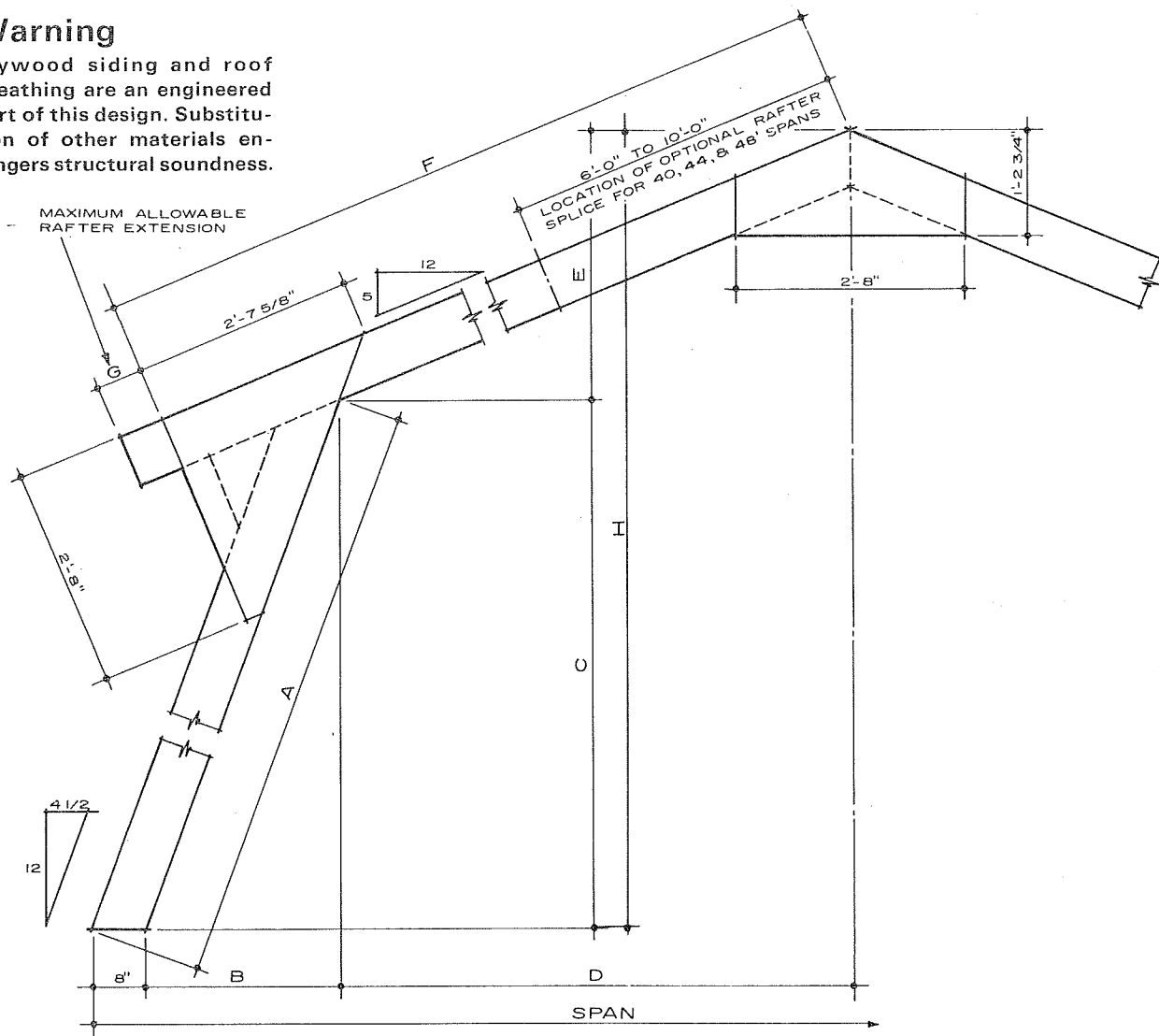


Fabrication details

2x8 slant leg

Warning

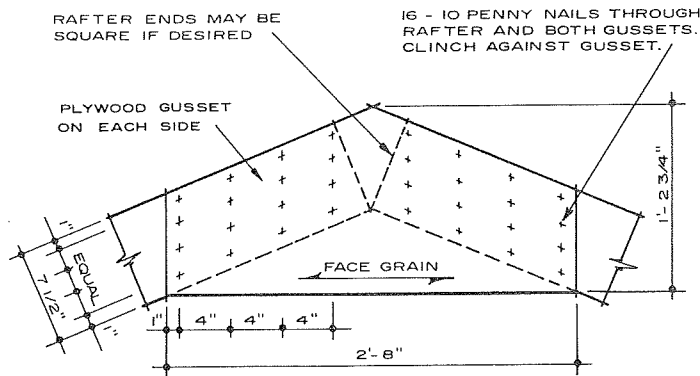
Plywood siding and roof sheathing are an engineered part of this design. Substitution of other materials endangers structural soundness.



Frame layout

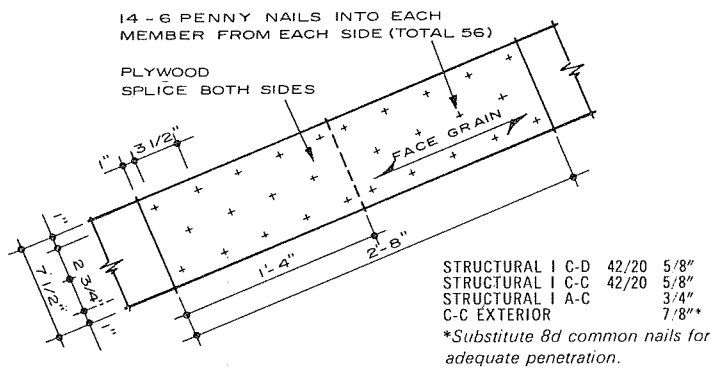
	A	6'- 0"	8'- 0"	10'- 0"	12'- 0"		A	6'- 0"	8'- 0"	10'- 0"	12'- 0"
All spans	B	2'- 0 1/4"	2'- 8 3/4"	3'- 5 1/8"	4'- 1 5/8"	All spans	B	2'- 0 1/4"	2'- 8 3/4"	3'- 5 1/8"	4'- 1 5/8"
	C	5'- 4 3/4"	7'- 3 1/4"	9'- 1 3/4"	11'- 0 1/4"		C	5'- 4 3/4"	7'- 3 1/4"	9'- 1 3/4"	11'- 0 1/4"
	G	7 1/4"	1'- 4 3/8"	2'- 1 1/2"	2'-10 5/8"		G	7 1/4"	1'- 4 3/8"	2'- 1 1/2"	2'-10 5/8"
24' span	D	9'- 3 3/4"	8'- 7 1/4"	7'-10 7/8"	7'- 2 3/8"	40' span	D	17'- 3 3/4"	16'- 7 1/4"	15'-10 7/8"	15'- 2 3/8"
	E	4'- 6 5/8"	4'- 3 1/8"	3'-11 5/8"	3'- 8 1/8"		E	7'-10 5/8"	7'- 7 1/8"	7'- 3 5/8"	7'- 0 1/8"
	F	12'- 4 3/4"	11'- 7 5/8"	10'-10 1/2"	10'- 1 3/8"		F	21'- 0 3/4"	20'- 3 5/8"	19'- 6 1/2"	18'- 9 3/8"
	H	9'-11 3/8"	11'- 6 3/8"	13'- 1 3/8"	14'- 8 3/8"		H	13'- 3 3/8"	14'-10 3/8"	16'- 5 3/8"	18'- 0 3/8"
32' span	D	13'- 3 3/4"	12'- 7 1/4"	11'-10 7/8"	11'- 2 3/8"	44' span	D	19'- 3 3/4"	18'- 7 1/4"	17'-10 7/8"	17'- 2 3/8"
	E	6'- 2 5/8"	5'-11 1/8"	5'- 7 5/8"	5'- 4 1/8"		E	8'- 8 5/8"	8'- 5 1/8"	8'- 1 5/8"	7'-10 1/8"
	F	16'- 8 3/4"	15'-11 5/8"	15'- 2 1/2"	14'- 5 3/8"		F	23'- 2 3/4"	22'- 5 5/8"	21'- 8 1/2"	20'-11 3/4"
	H	11'- 7 3/8"	13'- 2 3/8"	14'- 9 3/8"	16'- 4 3/8"		H	14'- 1 3/8"	15'- 8 3/8"	17'- 3 3/8"	18'-10 3/8"
36' span	D	15'- 3 3/4"	14'- 7 1/4"	13'-10 7/8"	14'- 2 3/8"	48' span	D	21'- 3 3/4"	20'- 7 1/4"	19'-10 7/8"	19'- 2 3/8"
	E	7'- 0 5/8"	6'- 9 1/8"	6'- 5 5/8"	6'- 2 1/8"		E	9'- 6 5/8"	9'- 3 3/8"	8'-11 5/8"	8'- 8 1/8"
	F	18'-10 3/4"	18'- 1 3/8"	17'- 4 1/2"	16'- 7 3/8"		F	25'- 4 3/4"	24'- 7 5/8"	23'-10 1/2"	23'- 1 3/8"
	H	12'- 5 3/8"	14'- 0 3/8"	15'- 7 3/8"	17'- 2 3/8"		H	14'-11 3/8"	16'- 6 3/8"	18'- 1 3/8"	19'- 8 3/8"

Crown gusset detail



STRUCTURAL I C-D	24/0	3/8"
STRUCTURAL I C-C	24/0	3/8"
STRUCTURAL I A-C		1/2"
C-C EXTERIOR		1/2"

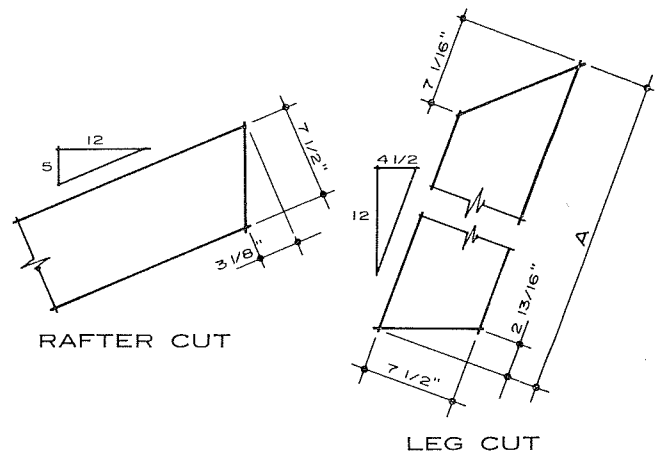
Optional rafter splice



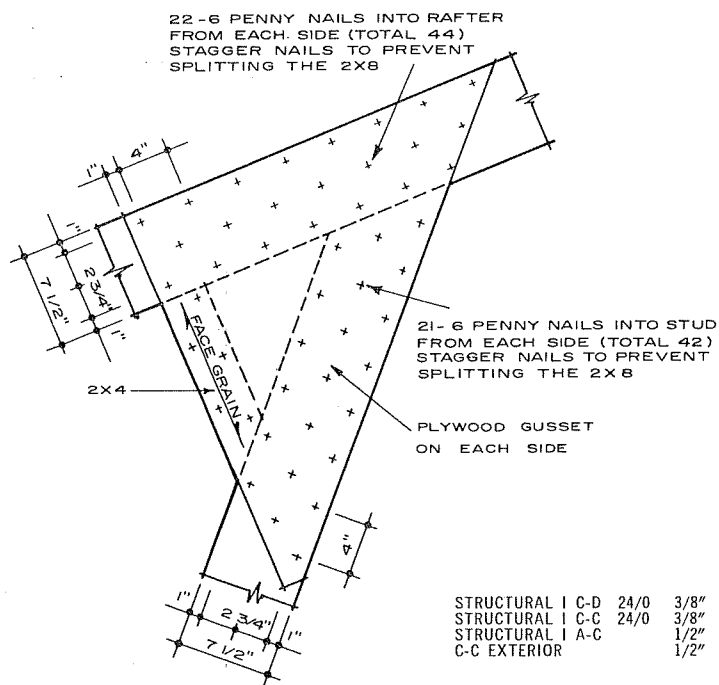
STRUCTURAL I C-D	42/20	5/8"
STRUCTURAL I C-C	42/20	5/8"
STRUCTURAL I A-C		3/4"
C-C EXTERIOR		7/8"

*Substitute 8d common nails for adequate penetration.

Lumber cuts

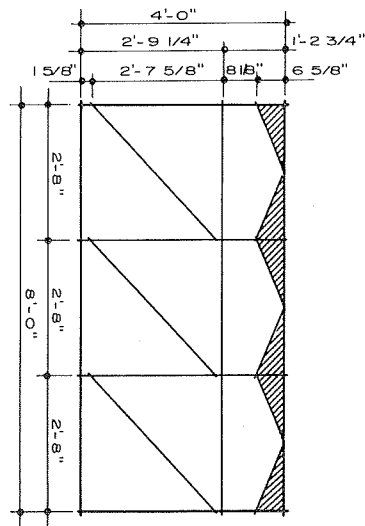


Haunch gusset detail



STRUCTURAL I C-D	24/0	3/8"
STRUCTURAL I C-C	24/0	3/8"
STRUCTURAL I A-C		1/2"
C-C EXTERIOR		1/2"

Plywood cutting diagram

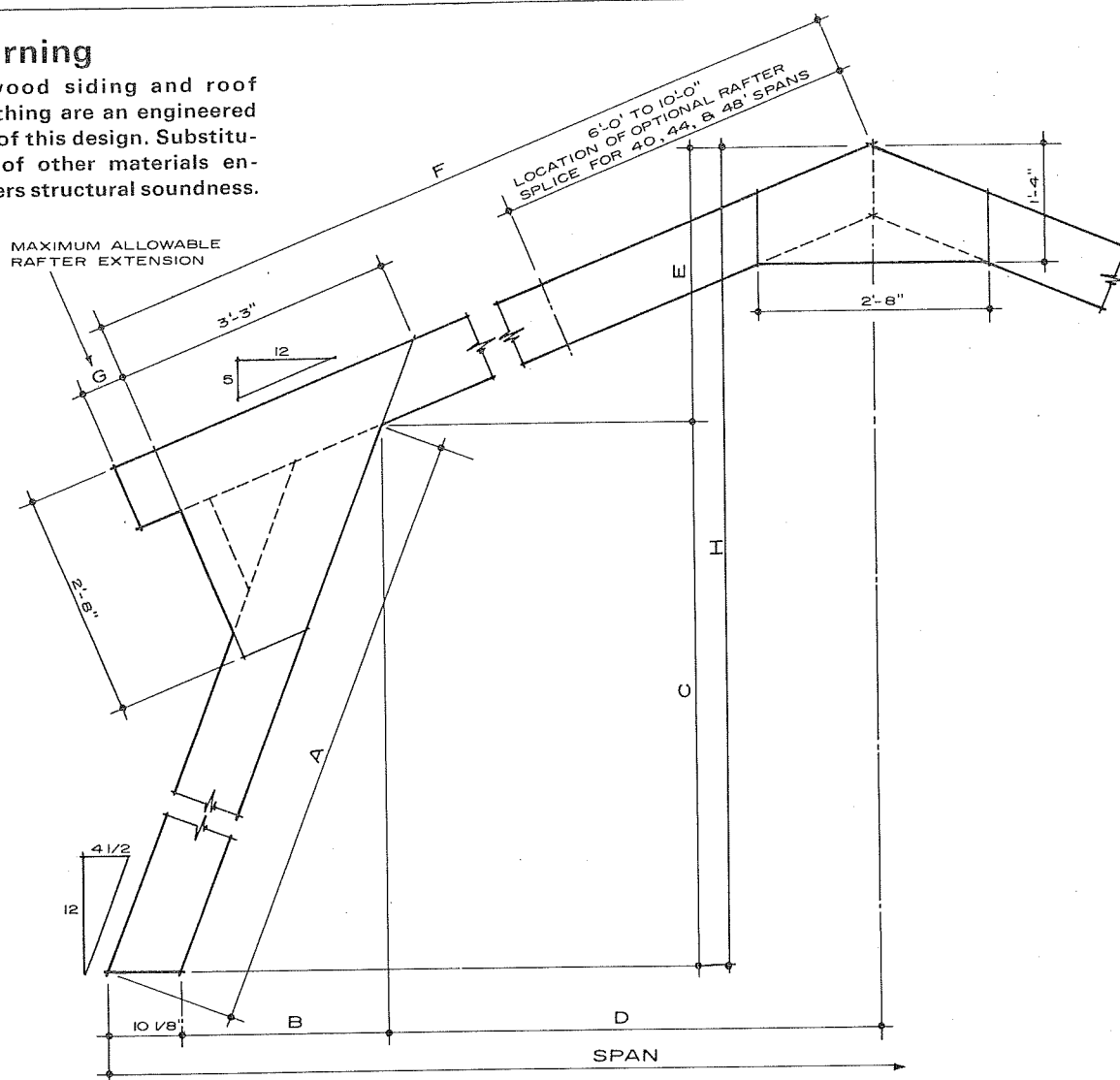


Fabrication details

2x10 slant leg

Warning

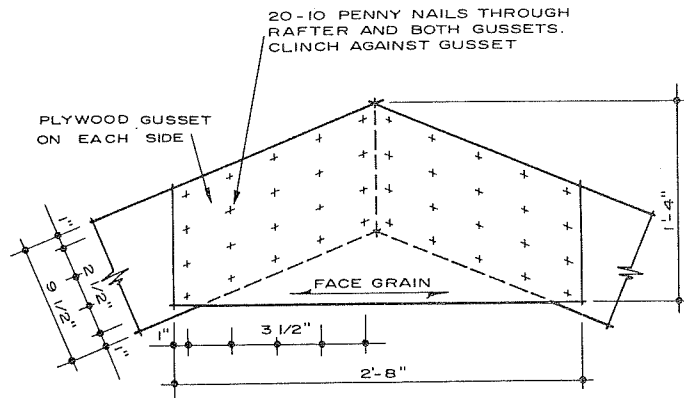
Plywood siding and roof sheathing are an engineered part of this design. Substitution of other materials endangers structural soundness.



Frame layout

	A	6'- 0"	8'- 0"	10'- 0"	12'- 0"		A	6'- 0"	8'- 0"	10'- 0"	12'- 0"
All spans	B	2'- 0"	2'- 8 1/2"	3'- 4 7/8"	4'- 1 3/8"	All spans	B	2'- 0"	2'- 8 1/2"	3'- 4 7/8"	4'- 1 3/8"
	C	5'- 4"	7'- 2 1/2"	9'- 1"	10'-11 1/2"		C	5'- 4"	7'- 2 1/2"	9'- 1"	10'-11 1/2"
	G	3"	1'- 0 1/2"	1'- 9 1/4"	2'- 6 3/8"		G	3"	1'- 0 1/8"	1'- 9 1/4"	2'- 6 3/8"
24' span	D	9'- 1 7/8"	8'- 5 3/8"	7'- 9"	7'- 0 1/2"	40' span	D	17'- 1 7/8"	16'- 5 3/8"	15'- 9"	15'- 0 1/2"
	E	4'- 8"	4'- 4 1/2"	4'- 1"	3'- 9 1/2"		E	8'- 0"	7'- 8 1/2"	7'- 5"	7'- 1 1/2"
	F	12'- 9"	11'-11 7/8"	11'- 2 3/4"	10'- 5 5/8"		F	21'- 5"	20'- 7 7/8"	19'-10 3/4"	19'- 1 5/8"
	H	10'- 0"	11'- 7"	13'- 2"	14'- 9"		H	13'- 4"	14'-11"	16'- 6"	18'- 1"
32' span	D	13'- 1 7/8"	12'- 5 3/8"	11'- 9"	11'- 0 1/2"	44' span	D	19'- 1 7/8"	18'- 5 3/8"	17'- 9"	17'- 0 1/2"
	E	6'- 4"	6'- 0 1/2"	5'- 9"	5'- 5 1/2"		E	8'-10"	8'- 6 1/2"	8'- 3"	7'-11 1/2"
	F	17'- 1"	16'- 3 7/8"	15'- 6 3/4"	14'- 9 5/8"		F	23'- 7"	22'- 9 7/8"	22'- 0 3/4"	21'- 3 5/8"
	H	11'- 8"	13'- 3"	14'-10"	16'- 5"		H	14'- 2"	15'- 9"	17'- 4"	18'-11"
36' span	D	15'- 1 7/8"	14'- 5 3/8"	13'- 9"	13'- 0 1/2"	48' span	D	21'- 1 7/8"	20'- 5 3/8"	19'- 9"	19'- 0 1/2"
	E	7'- 2"	6'-10 1/2"	6'- 7"	6'- 3 1/2"		E	9'- 8"	9'- 4 1/2"	9'- 1"	8'- 9 1/2"
	F	19'- 3"	18'- 5 7/8"	17'- 8 3/4"	16'-11 5/8"		F	25'- 9"	24'-11 7/8"	24'- 2 3/4"	23'- 5 5/8"
	H	12'- 6"	14'- 1"	15'- 8"	17'- 3"		H	15'- 0"	16'- 7"	18'- 2"	19'- 9"

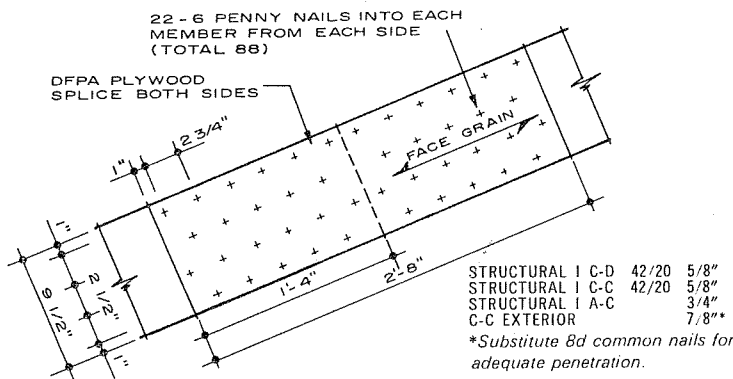
Crown gusset detail



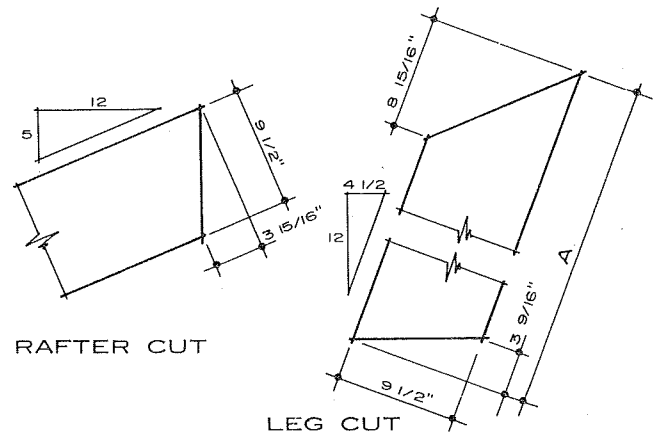
STRUCTURAL I C-D 32/16 1/2"
STRUCTURAL I C-C 32/16 1/2"
STRUCTURAL I A-C 1/2"
C-C EXTERIOR 5/8"

*Substitute 12d common nails for
adequate penetration.

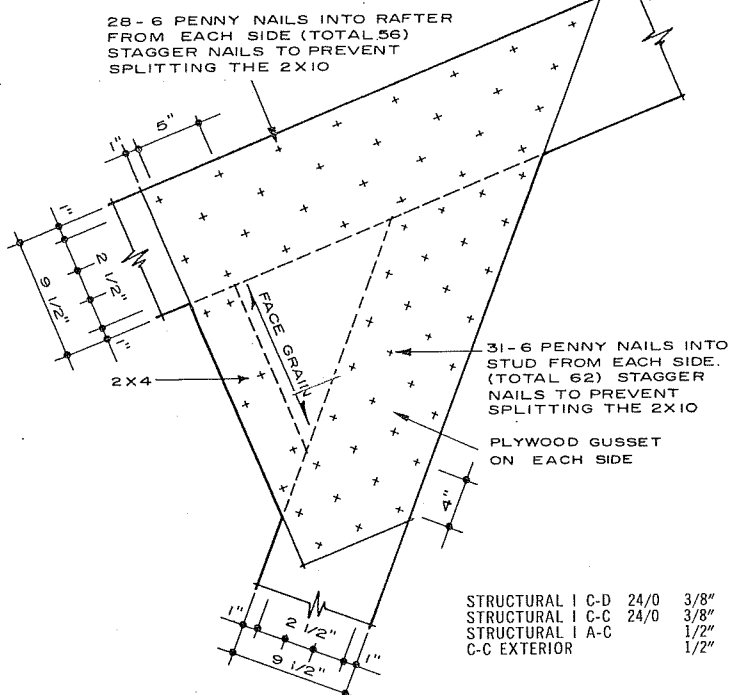
Optional rafter splice



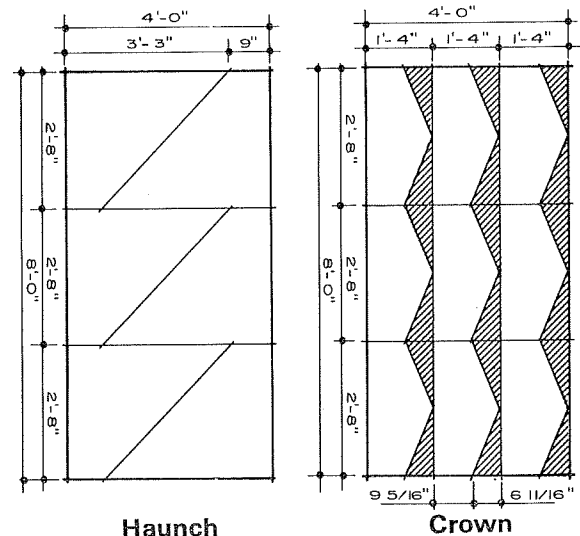
Lumber cuts



Haunch gusset detail



Plywood cutting diagram

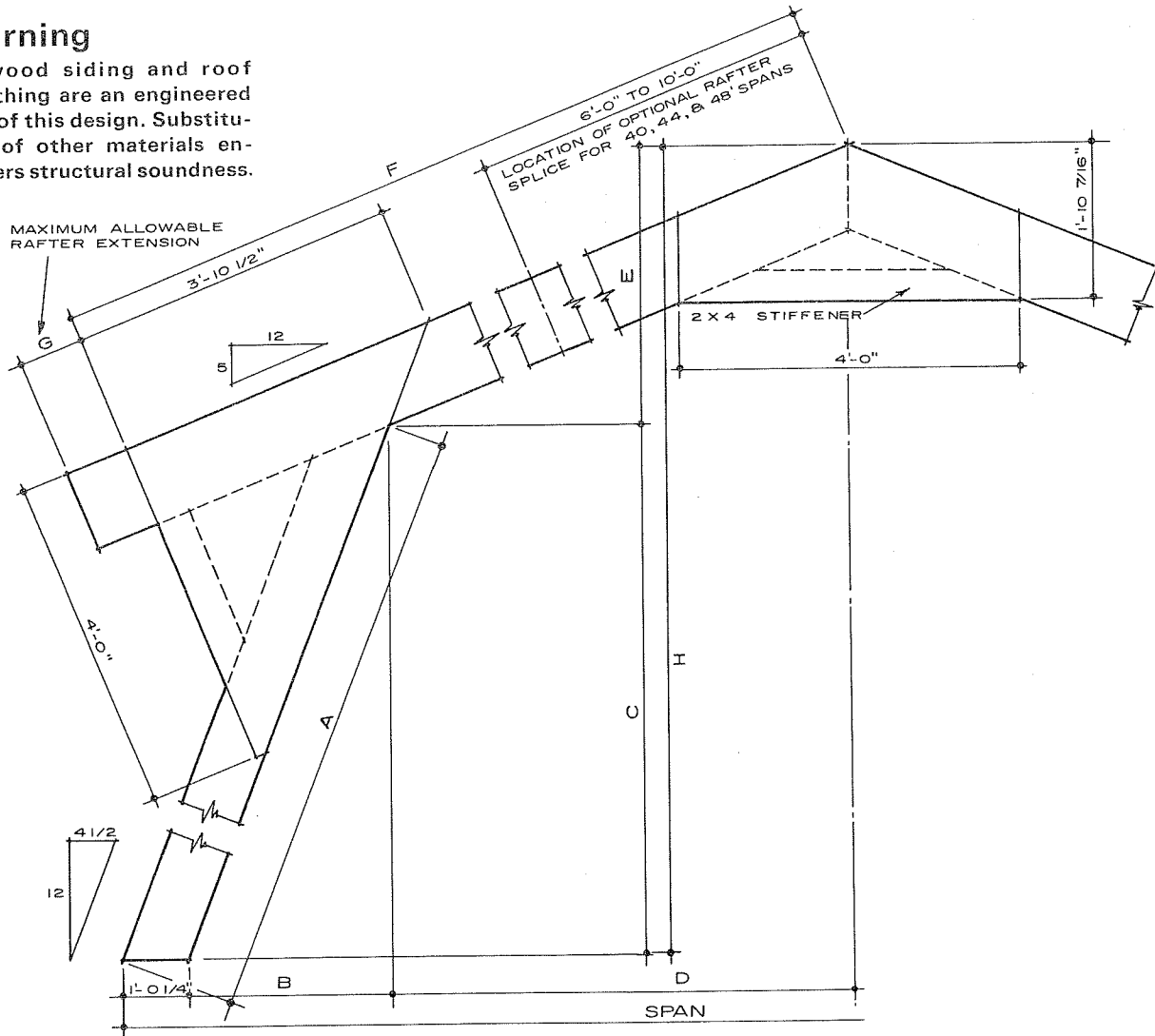


Fabrication details

2x12 slant leg

Warning

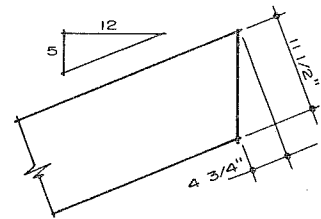
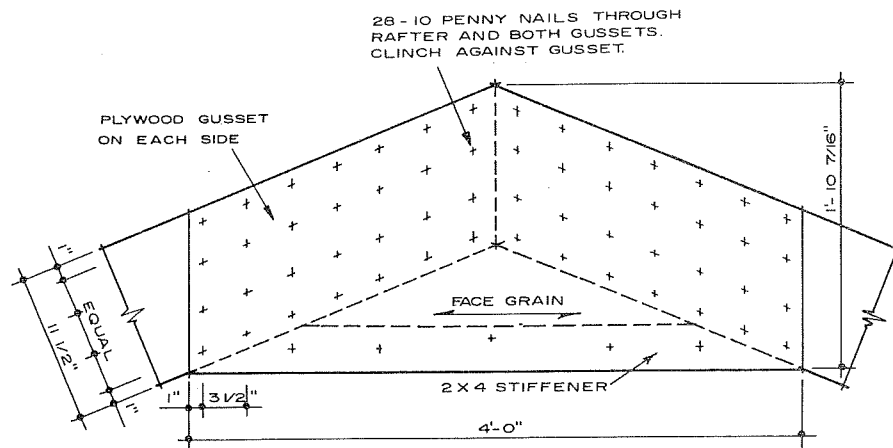
Plywood siding and roof sheathing are an engineered part of this design. Substitution of other materials endangers structural soundness.



Frame layout

	A	6'- 0"	8'- 0"	10'- 0"	12'- 0"		A	6'- 0"	8'- 0"	10'- 0"	12'- 0"
All spans	B	1'-11 $\frac{3}{4}"$	2'- 8 $\frac{1}{8}"$	3'- 4 $\frac{5}{8}"$	4'- 1"	All spans	B	1'-11 $\frac{3}{4}"$	2'- 8 $\frac{1}{8}"$	3'- 4 $\frac{5}{8}"$	4'- 1"
	C	5'- 3 $\frac{3}{8}"$	7'- 1 $\frac{7}{8}"$	9'- 0 $\frac{1}{4}"$	10'-10 $\frac{3}{4}"$		C	5'- 3 $\frac{3}{8}"$	7'- 1 $\frac{7}{8}"$	9'- 0 $\frac{1}{4}"$	10'-10 $\frac{3}{4}"$
	G	0"	7 $\frac{5}{8}"$	1'- 4 $\frac{3}{4}"$	2'- 2"		G	0"	7 $\frac{5}{8}"$	1'- 4 $\frac{3}{4}"$	2'- 2"
24' span	D	9'- 0"	8'- 3 $\frac{1}{2}"$	7'- 7 $\frac{1}{2}"$	6'-10 $\frac{5}{8}"$	40' span	D	17'- 0"	16'- 3 $\frac{1}{2}"$	15'- 7 $\frac{1}{8}"$	14'-10 $\frac{5}{8}"$
	E	4'- 9 $\frac{1}{2}"$	4'- 6"	4'- 2 $\frac{3}{8}"$	3'-10 $\frac{7}{8}"$		E	8'- 1 $\frac{1}{2}"$	7'-10"	7'- 6 $\frac{3}{8}"$	7'- 2 $\frac{7}{8}"$
	F	13'- 1 $\frac{1}{2}"$	12'- 4 $\frac{3}{8}"$	11'- 7 $\frac{1}{4}"$	10'-10"		F	21'- 9 $\frac{1}{2}"$	21'- 0 $\frac{3}{8}"$	20'- 3 $\frac{1}{4}"$	19'- 6"
	H	10'- 0 $\frac{7}{8}"$	11'- 7 $\frac{7}{8}"$	13'- 2 $\frac{5}{8}"$	14'- 9 $\frac{5}{8}"$		H	13'- 4 $\frac{7}{8}"$	14'-11 $\frac{7}{8}"$	16'- 6 $\frac{5}{8}"$	18'- 1 $\frac{5}{8}"$
32' span	D	13'- 0"	12'- 3 $\frac{1}{2}"$	11'- 7 $\frac{1}{8}"$	10'-10 $\frac{5}{8}"$	44' span	D	19'- 0"	18'- 3 $\frac{1}{2}"$	17'- 7 $\frac{1}{8}"$	16'-10 $\frac{5}{8}"$
	E	6'- 5 $\frac{1}{2}"$	6'- 2"	5'-10 $\frac{3}{8}"$	5'- 6 $\frac{7}{8}"$		E	8'-11 $\frac{1}{2}"$	8'- 8"	8'- 4 $\frac{3}{8}"$	8'- 0 $\frac{7}{8}"$
	F	17'- 5 $\frac{1}{2}"$	16'- 8 $\frac{3}{8}"$	15'-11 $\frac{1}{4}"$	15'- 2"		F	23'-11 $\frac{1}{2}"$	23'- 2 $\frac{3}{8}"$	22'- 5 $\frac{1}{4}"$	21'- 8"
	H	11'- 8 $\frac{7}{8}"$	13'- 3 $\frac{7}{8}"$	14'-10 $\frac{5}{8}"$	16'- 5 $\frac{5}{8}"$		H	14'- 2 $\frac{7}{8}"$	15'- 9 $\frac{7}{8}"$	17'- 4 $\frac{5}{8}"$	18'-11 $\frac{5}{8}"$
36' span	D	15'- 0"	14'- 3 $\frac{1}{2}"$	13'- 7 $\frac{1}{8}"$	12'-10 $\frac{5}{8}"$	48' span	D	21'- 0"	20'- 3 $\frac{1}{2}"$	19'- 7 $\frac{1}{8}"$	18'-10 $\frac{5}{8}"$
	E	7'- 3 $\frac{3}{8}"$	7'- 0"	6'- 8 $\frac{3}{8}"$	6'- 4 $\frac{7}{8}"$		E	9'- 9 $\frac{1}{2}"$	9'- 6"	9'- 2 $\frac{3}{8}"$	8'-10 $\frac{7}{8}"$
	F	19'- 7 $\frac{1}{2}"$	18'-10 $\frac{3}{8}"$	18'- 1 $\frac{1}{4}"$	17'- 4"		F	26'- 1 $\frac{1}{2}"$	25'- 4 $\frac{3}{8}"$	24'- 7 $\frac{1}{4}"$	23'-10"
	H	12'- 6 $\frac{7}{8}"$	14'- 1 $\frac{7}{8}"$	15'- 8 $\frac{5}{8}"$	17'- 3 $\frac{5}{8}"$		H	15'- 0 $\frac{7}{8}"$	16'- 7 $\frac{7}{8}"$	18'- 2 $\frac{5}{8}"$	19'- 9 $\frac{5}{8}"$

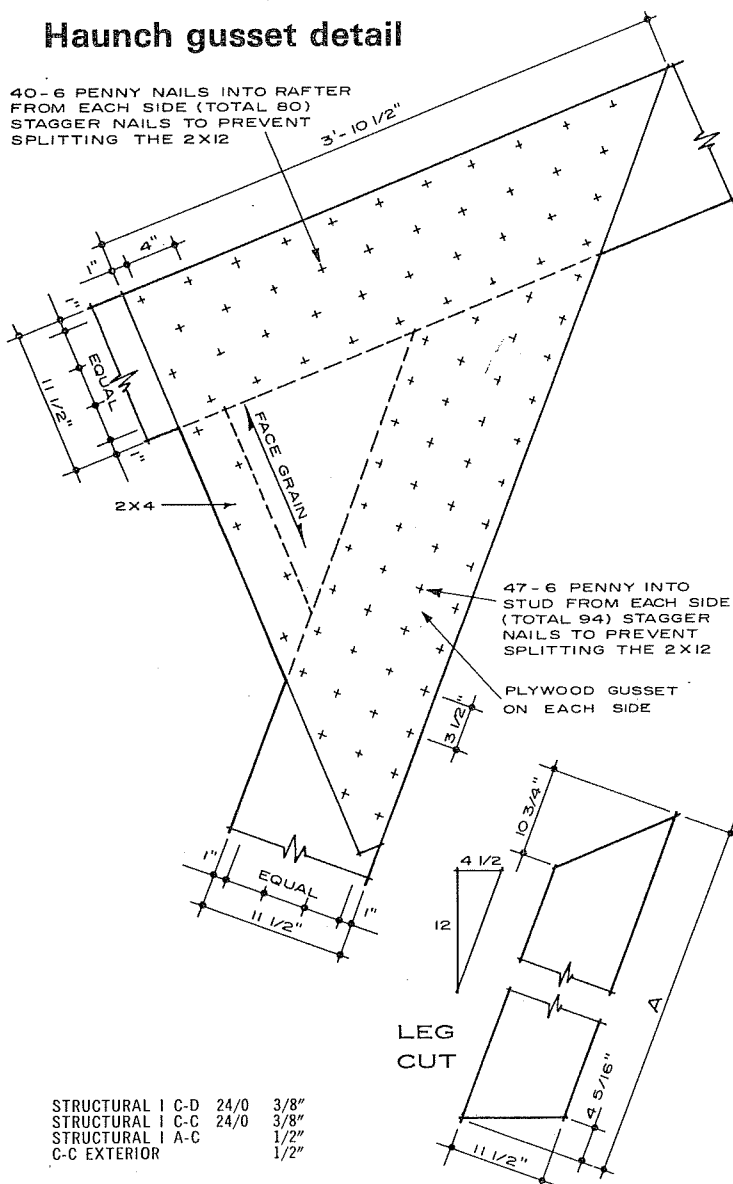
Crown gusset detail



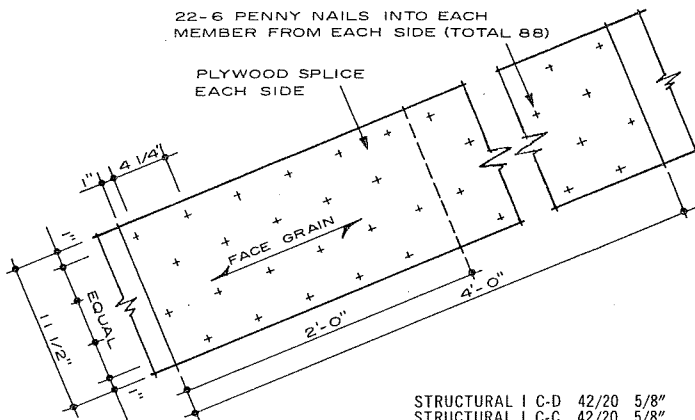
RAFTER CUT

STRUCTURAL I C-D	24/0	3/8"
STRUCTURAL I C-C	24/0	3/8"
STRUCTURAL I A-C		1/2"
C-C EXTERIOR		1/2"

Haunch gusset detail



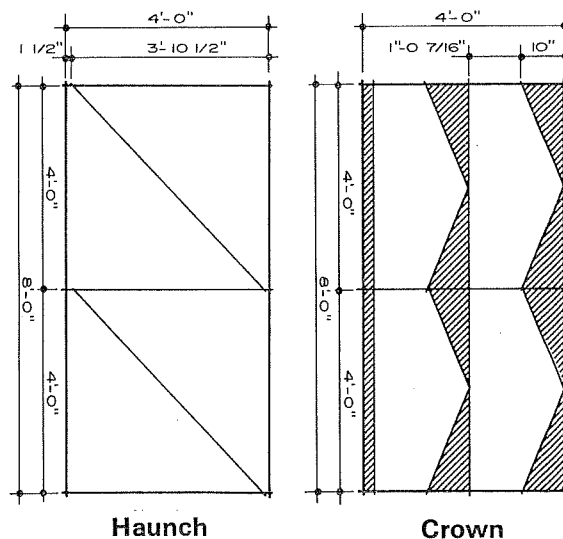
Optional rafter splice



STRUCTURAL I C-D	42/20	5/8"
STRUCTURAL I C-C	42/20	5/8"
STRUCTURAL I A-C		3/4"
C-C EXTERIOR		7/8"

*Substitute 8d common nails for adequate penetration.

Plywood cutting diagram

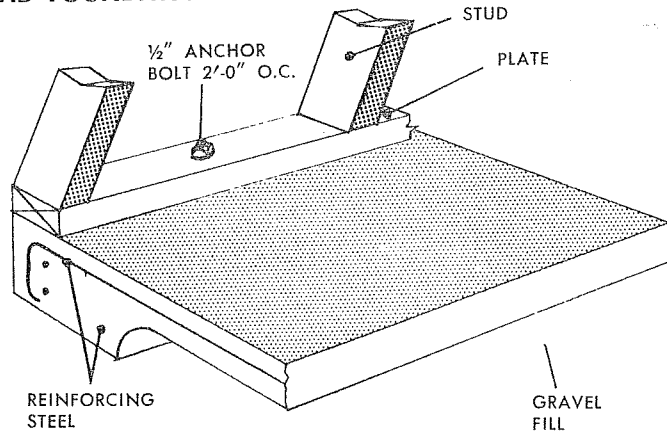


STRUCTURAL I C-D	24/0	3/8"
STRUCTURAL I C-C	24/0	3/8"
STRUCTURAL I A-C		1/2"
C-C EXTERIOR		1/2"

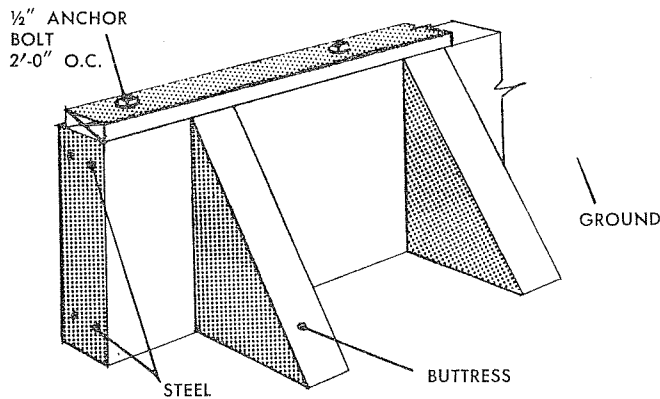
STEP-BY-STEP ERECTION OF A RIGID FRAME STRUCTURE

STEP 1: FOUNDATIONS (3 ALTERNATE METHODS)

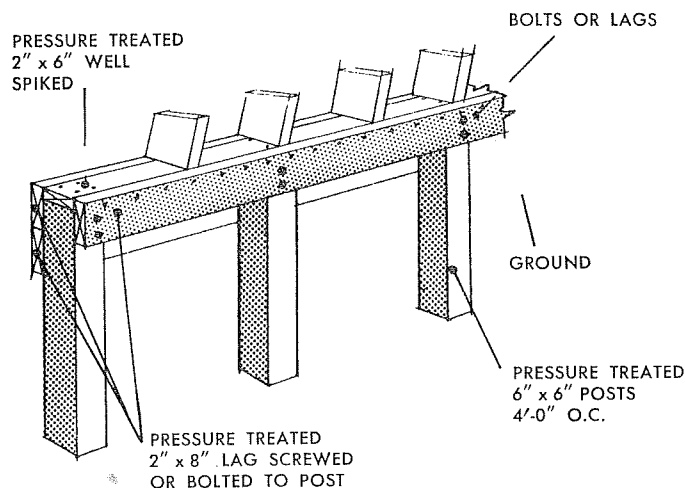
SLAB FOUNDATION



WALL FOUNDATION



POST AND BEAM



As with any building the site should be selected carefully, considering the slope of the land, relation to other buildings and possible uses of the building.

Since conditions and functions vary greatly the foundation must be designed to meet the varying purposes of each building. It must be capable of supporting the vertical load plus resisting about 700 pounds of outward thrust at each rigid frame.

The slab foundation, as illustrated, is a method of letting the slab reinforcing steel act as a tie rod. This "tie rod" joins the walls so that the thrust of one counteracts the other.

If the building is to be heated, the edge of the slab should be insulated. Note that 1/2" anchor bolts are spaced 2' to fasten plate down. The slab type foundation will give a simple economical foundation and permanent slab floor in one unit.

The buttresses of the wall foundation carry the outward thrust of the rigid frames directly to the soil. This type of foundation will serve when no concrete floor is desired or when soil conditions forbid use of a slab. Again 1/2" anchor bolts at a spacing of 2' are required.

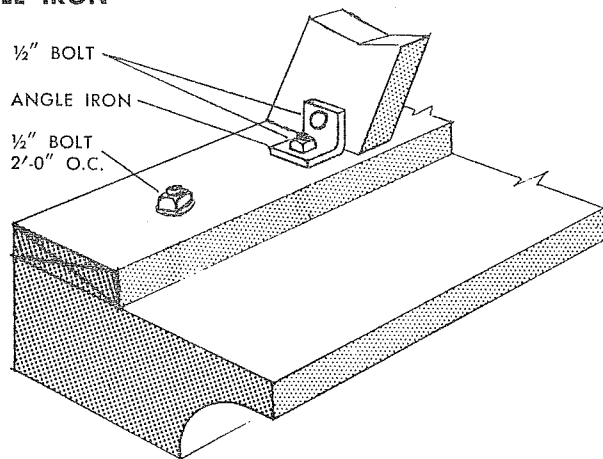
Note: Footings and wall foundations require form work that can easily be made with plywood. With a little advance planning the plywood used in the form work can be used later in some portion of the building.

The post and beam system makes a very economical foundation. It utilizes pressure treated posts and planks. This foundation is recommended when concrete is not readily available. The length of posts required will depend upon soil conditions. Pressure treated planks are lag screwed or bolted to the sides of the post so that they extend into the soil to resist the thrust of the rigid frames. Placing the planks partially in the ground helps to eliminate drafts in the finished building.

While only three basic foundation ideas are illustrated, there are other suitable types to meet special conditions. Whatever type of foundation is used it must be designed carefully to carry the loads. Before building, local building authorities should be consulted.

STEP 2: FOUNDATION FASTENING (3 METHODS) (SEE ALSO PAGE 10)

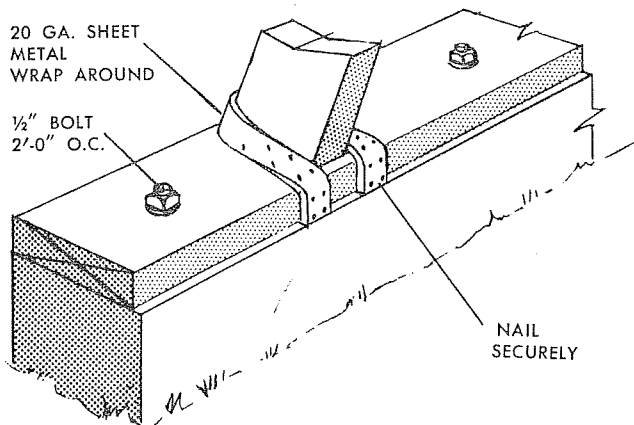
ANGLE IRON



Rigid frames must be anchored securely to the plate to resist the outward thrust at the base. Merely toe-nailing the stud to the plate is *not* sufficient.

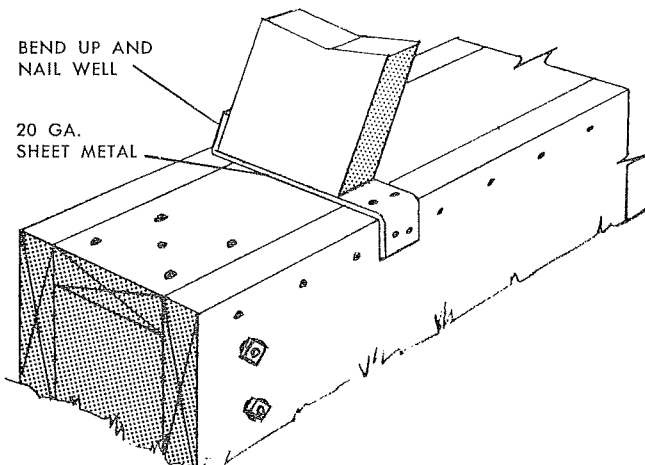
A short section of angle iron fastened to the plate and the stud will work well. Half inch bolts are recommended for fastening. If the bolts used to anchor the plate are positioned accurately they may also serve to fasten the angle iron.

WRAP FASTENER



The sheet metal connectors illustrated can be purchased or easily made by the builder. Twenty gauge metal is desirable since it can be nailed without drilling. The use of galvanized sheet metal prevents rusting. Connectors should be nailed securely with ample nails. Care should be taken not to split the stud or the plate.

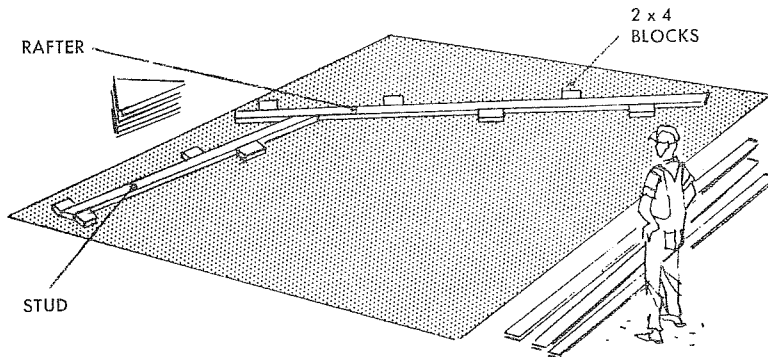
PLATE FASTENER



Various commercially available stud sockets, and framing anchors may be used, providing they are capable of withstanding about 700 pounds of thrust.

STEP-BY-STEP ERECTION OF A RIGID FRAME STRUCTURE

STEP 3: LAYOUT OF RIGID FRAMES

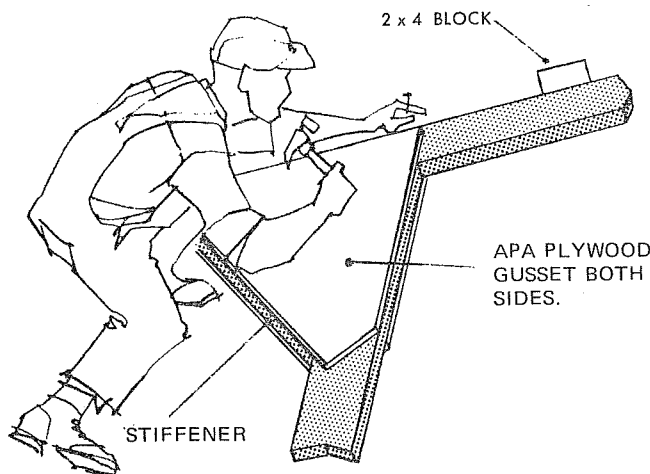


First cut plywood and lumber for one-half of a rigid frame and before cutting the balance of the material check it in an assembly jig.

Lay out the jig as shown. A level floor or large platform should be used. A temporary working surface can be made by laying several sheets of plywood on a level piece of ground. A raised platform on posts will make the job much easier.

Nail 2" x 4" blocks as illustrated to hold framing members in the correct position. Place members in position, and check all dimensions given on the plan. Make sure that the plywood gusset fits accurately. Do not nail these members together. They should be marked and used as a pattern for cutting the other members. All members may now be pre-cut.

STEP 4: NAILING OF GUSSETS

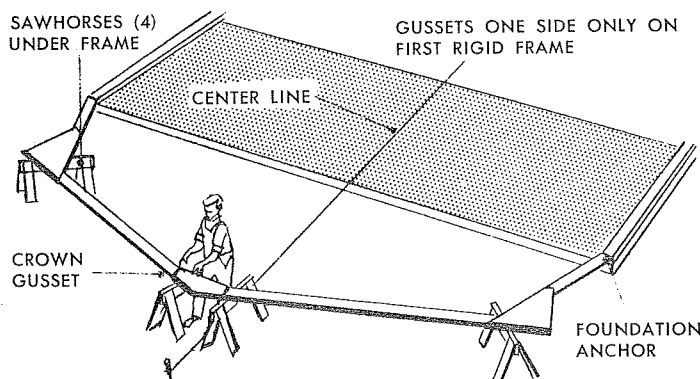


Arch halves are fabricated by nailing a plywood gusset to each side of the haunch. For easy nail spacing, a paper or cardboard stencil can be made with a 1/4" hole at each nail location. With this stencil and stencil paint, or a similar marking device, marks can be made where required. This saves time and eliminates nailing errors.

Even though it's nearly impossible to split plywood by nailing, gusset nails should be staggered slightly to prevent splitting the lumber members. At this point be certain you plan ahead for doorways. See page 31 for doorway details.

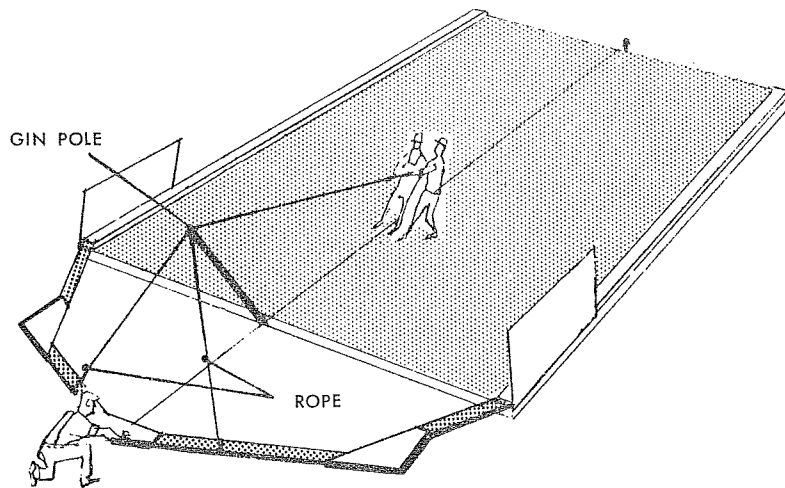
It is easier to assemble rigid frame halves only at this time. The crown gusset will be applied just before raising the frames. The first frame has gussets only on the inside face since the plywood end wall will serve as the outside gusset.

STEP 5: LAYOUT OF RAFTER HALVES AND ATTACHING OF CROWN GUSSET



Two halves may now be placed on sawhorses as illustrated. The base of the stud should be at the edge of the plate. The use of a center line will help to properly position the halves. Use 10d nails to nail the crown gusset since it is impractical to nail the gusset from both sides and 10d nails will go through the rafter and both gussets. The nails can then be clinched on the lower side. A pair of clamps will help hold the lower gusset while the first nails are driven.

STEP 6: GIN POLE ERECTION OF FIRST FRAME

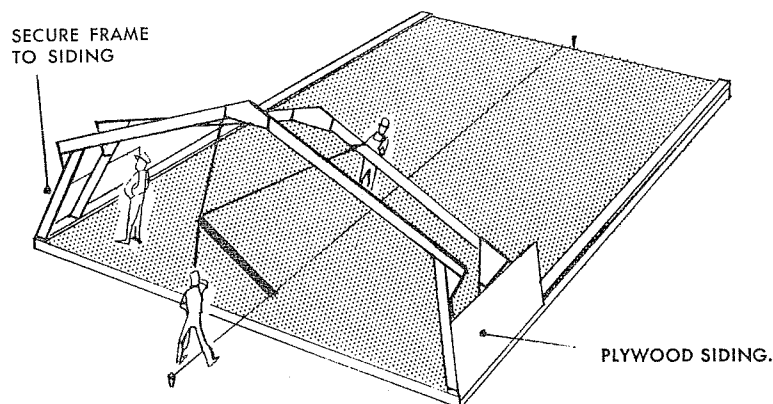


The frame is now ready for raising. Stud anchors should be located and fastened to the plate. Two sheets of plywood can be nailed to the plate as illustrated. These will serve as braces when the rigid frames are raised. They also are part of the finished building. Nail with 6d nails 3" o.c.

Three men working with a simple gin pole arranged as illustrated can easily raise and secure rigid frame units in place. The pole should be slightly shorter than the distance from the ground to the crown gusset. Fasten a rope bridle to the frame about 8 to 10 feet from the crown and pass over the gin pole at about 20 degrees off the perpendicular.

When the frame is vertical two men carefully plumb the legs and fasten to the plywood wall panels. Nail with 6d nails 6" o.c.

STEP 7: ERECTION OF SUCCEEDING FRAMES

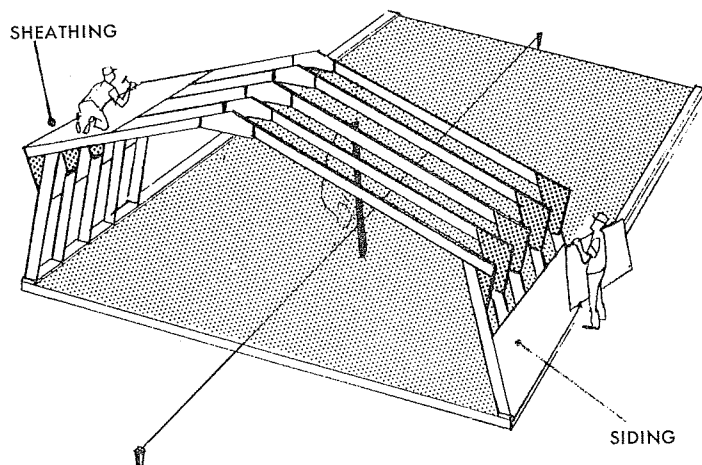


The second frame is laid out and raised from inside the building. Follow the same procedure as for the first rigid frame.

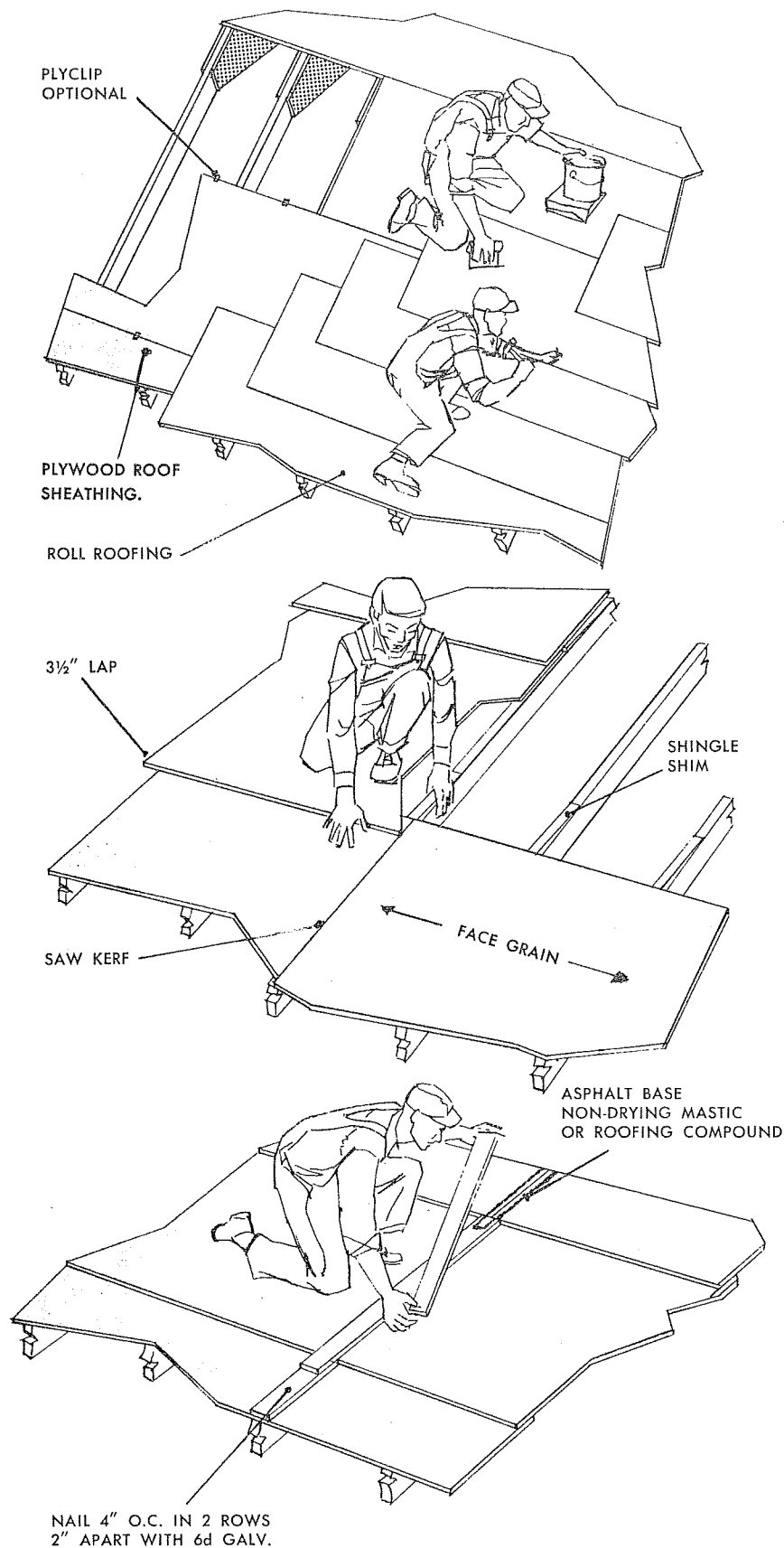
Each frame is plumbed as it is raised and fastened to the plywood siding. Plywood's large panel size serves both as a temporary and permanent bracing. This eliminates any need for additional braces in the building. Once several frames are up, apply a panel of plywood roof sheathing at the eave line.

This will prevent the possibility of the frames being blown down by wind before the roof is fastened securely in place.

Mechanical equipment such as a farm tractor with loader can also be helpful in speeding the erection job.



STEP 8: ROOFING DETAILS



Big 4 x 8 plywood panels easily provide the diaphragm strength and rigidity a building of this type requires.

An economical watertight roof can be obtained by sheathing the roof with plywood roof sheathing and covering with roll roofing, asphalt shingles or wood shingles. Plyclips may be used to join panel edges for additional stiffness. Face grain of the panels must be across the rafters as the plywood is stiffer when applied in this manner. Stagger panel joints. Nail panels with 6d nails 6" on centers on all supported panel edges and 12" on centers on intermediate rafters.

Plywood's excellent nail holding properties and high dimensional stability insure a solid, flat and nonbuckling roof that stays down.

ALTERNATE ROOFING METHOD

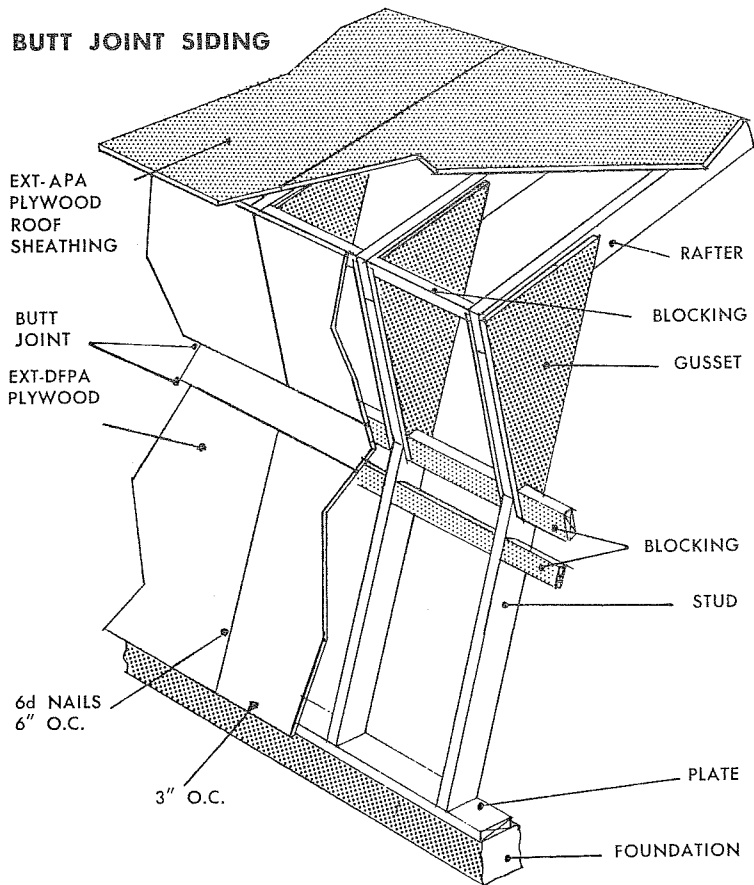
Exterior plywood can be applied as giant shingles on buildings when a weather resistant roof is satisfactory and minor leaks occurring are not objectionable. The degree of water-tightness obtained depends on the quality of application, workmanship and the joint sealer used.

To apply an exposed plywood roof, nail a course of panels along the eave line with 6d galvanized nails with a nailing schedule the same as used on applying roof sheathing. Place a shingle shim on each rafter above top panel edge. Run a power saw kerf between vertical panel joints to allow for expansion. Lap the second course of panels 3 1/2" over the first course with a generous bead of asphalt base, non-drying mastic under the lap. Repeat until roof is covered.

Rip 3" wide batten strips 4' long from a 3/8" C-C Exterior panel with the face grain running lengthwise of the batten. Fill the saw kerf with a generous application of non-drying asphalt base roofing compound as well as thoroughly coating the area to be covered by the batten. Apply the battens as illustrated, nailing 4" on centers with 6d galvanized nails in two rows, 2" apart, slanted to catch rafter. Fill any open panel defects with roofing compound to avoid panel leaks.

STEP 9: SIDING DETAILS

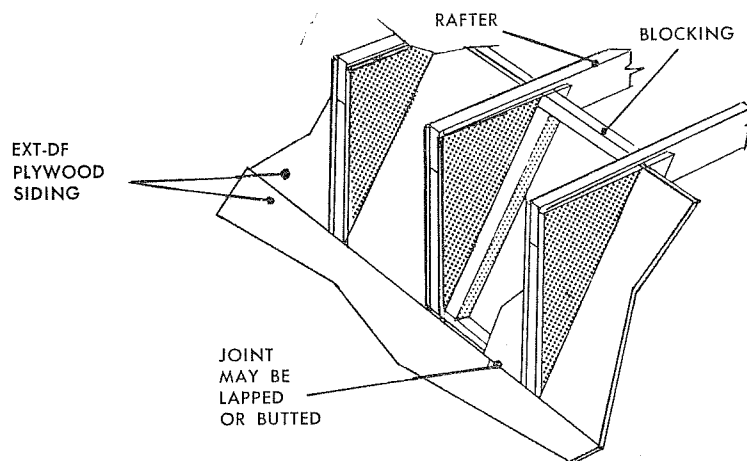
BUTT JOINT SIDING



Plywood is the only material that easily and fully develops the strength of a rigid frame building. And the best method for applying plywood siding depends largely upon the intended use of the building. The methods illustrated on this page are adequate for most utility buildings. The butt joint system requires a minimum of cutting. Plywood panels should be nailed with 6d nails 6" o.c. around the outside of the panel and 12" o.c. on intermediate studs.

If a more weatherproof wall is needed, a system similar to the giant shingle roof can be used. This lap and batten system is illustrated on page 28.

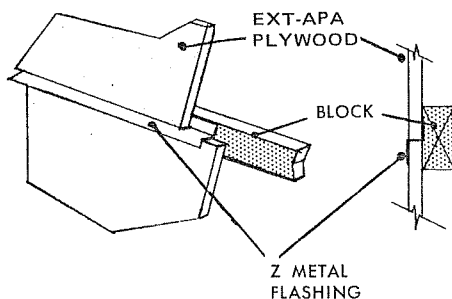
ALTERNATE SIDING METHODS



By nailing blocking to the sides of the gusset the siding can extend straight up between the frames to give a continuous slanted wall. This siding method as illustrated makes it possible to use up small plywood cuttings. Glass may be substituted to give a low cost window.

Construction with plywood provides a draft free building because the large panel size means a minimum number of joints.

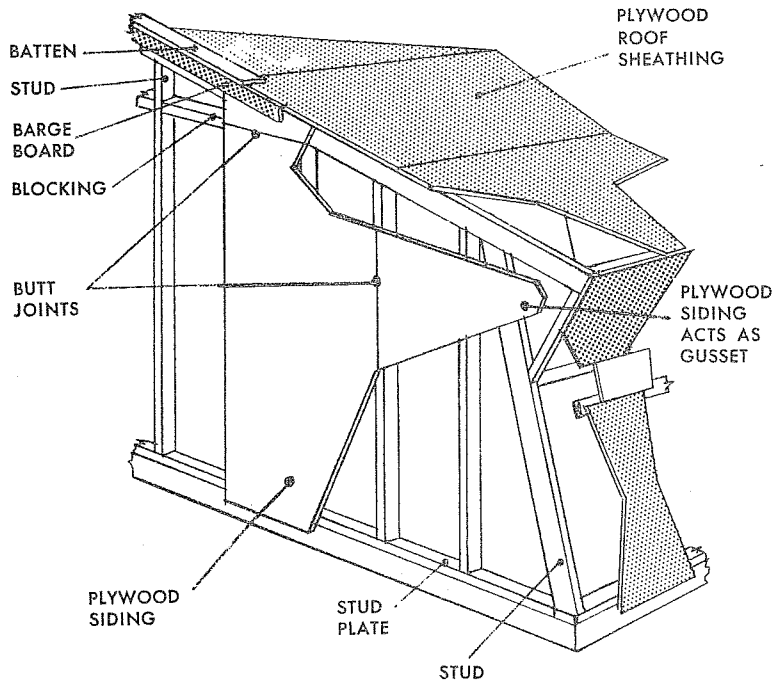
ALTERNATE PLYWOOD JOINT TREATMENT



A bent metal Z flashing will give a very weather resistant horizontal joint. Light gauge galvanized steel or aluminum should be used.

STEP-BY-STEP ERECTION OF A RIGID FRAME STRUCTURE

STEP 10: END WALLS



End walls are conventional stud wall construction, with plywood as a "must" for end wall siding because it acts as a gusset for the end rigid frame.

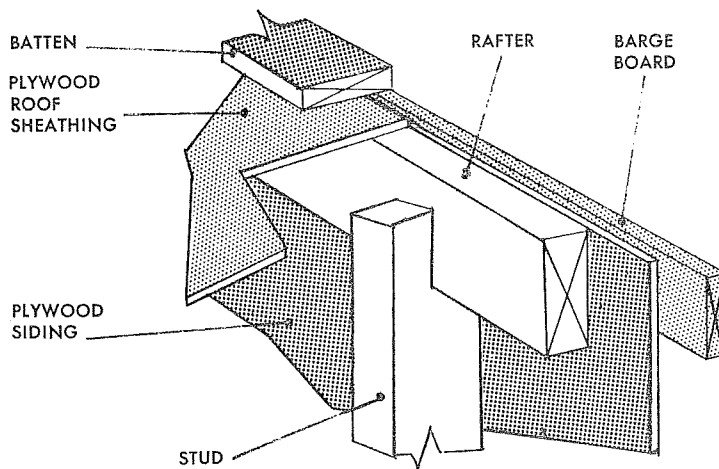
Nailing of the frame gusset should be duplicated in this area. Space the studs 24" o.c. and block as required at the horizontal joints. Fasten your plywood siding in place with 6d galvanized nails. Space them 6" apart around the panel edges and 12" apart on intermediate supports. Butt joints, like those shown here, will be satisfactory for most utility buildings.

A Z flashing as shown on page 29 may be used at the horizontal joint for more weather resistance.

If an extremely weatherproof end wall is desired the giant shingle system as illustrated on page 28 should be used.

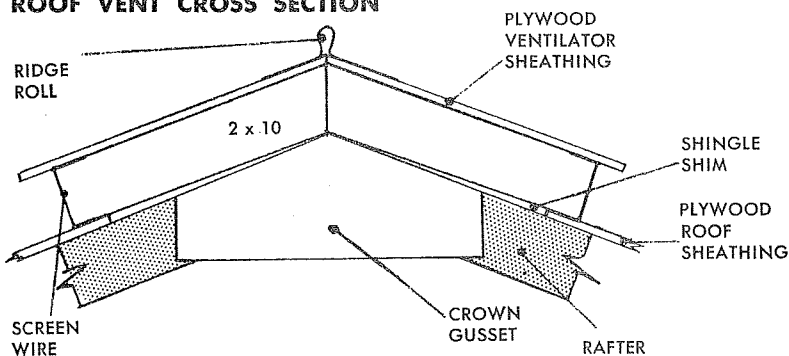
If desired the entire end wall may be omitted without weakening the structure. But the gussets must be applied to the outside face of the rigid frame.

DETAIL AT TOP OF STUDS (INSIDE)



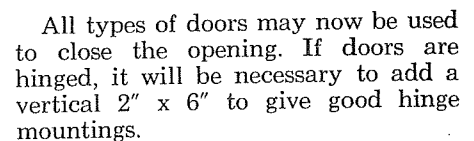
End wall studs are notched to fasten to the rafter as illustrated. The batten and barge board as illustrated give a neat inexpensive joint.

STEP 11: OPENINGS ROOF VENT CROSS SECTION



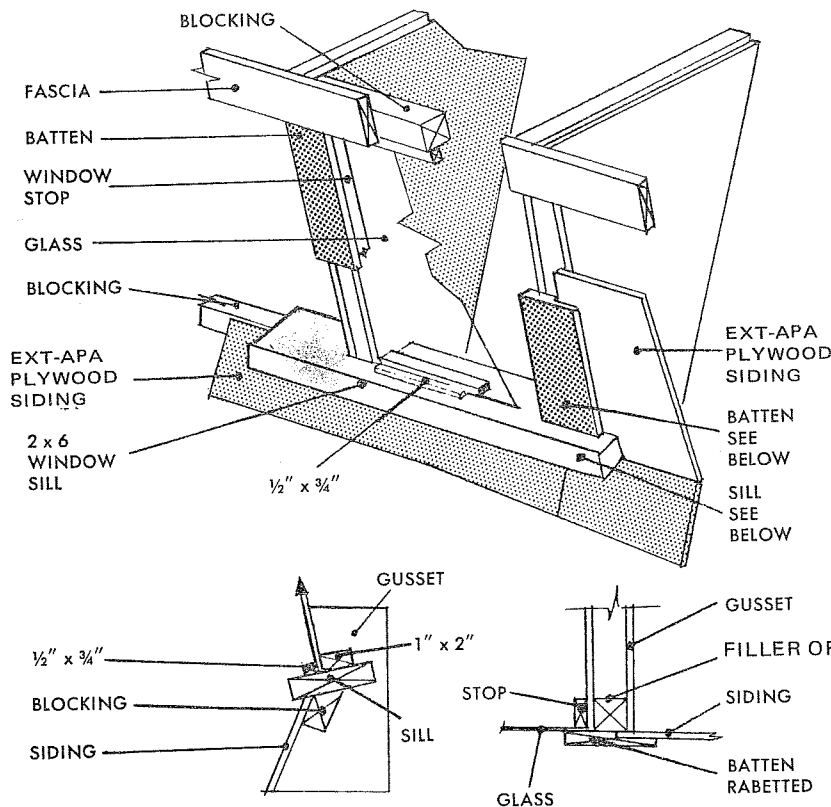
A simple plywood ridge ventilator (shown here and on the cover) is best when ventilation is desired. Simple plywood doors, when added to the ventilator prevent excessive drafts. Screening will prevent birds nesting.

(TRIANGULAR DOOR POST)



STEP 11: OPENINGS (continued)

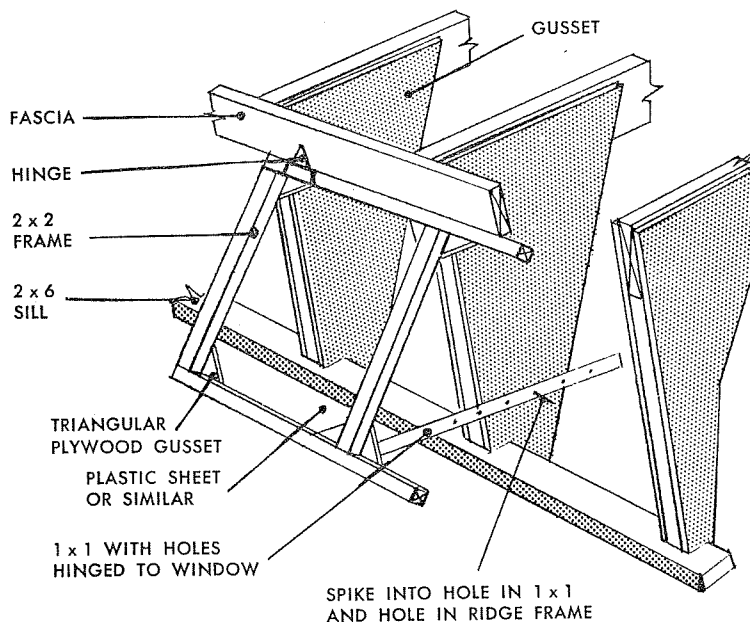
WINDOW INSTALLATION DETAILS



Endwall windows, if desired, are installed as in conventional stud construction. For side windows large panes of glass may be set with glazing compound and wood stops as illustrated. The 2" x 6" sill is notched to fit around the rigid frames. Tipping the sill as shown insures drainage. It is placed perpendicular to the outside edge of the gusset. The 1" x 4" batten at the edge of the windows must be rabbeted as shown to catch both the siding and the glass. The windows as shown could run the entire length of the building.

If desired, a standard sash unit may be installed in a similar manner.

ALTERNATE WINDOW DETAIL



For some buildings it will be necessary to have windows that may be opened for ventilation. A simple window frame may be built of 2" x 2" as shown. Small triangular gussets at each corner make the window frame very solid. The frame may then be covered with plastic or similar inexpensive sheet material.

The 1" x 1" with holes and a spike serves as a prop to hold the window open or latch it when closed. The 1" x 1" is hinged to the frame.